

Recent Advances in Radiative Cooling: From Fundamentals to Commercial Applications

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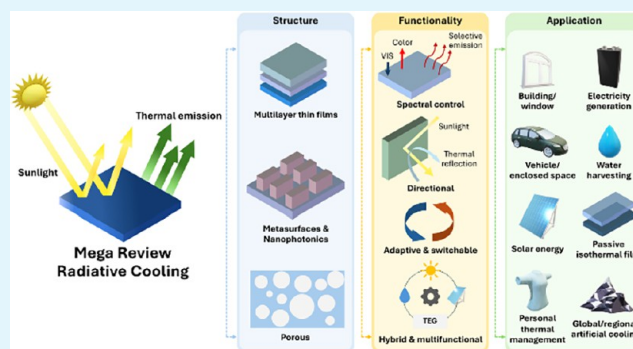
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ABSTRACT: Radiative cooling (RC) is a sustainable technology that passively lowers the temperature of terrestrial objects through thermal radiation, dissipating heat into outer space via the atmospheric window, unlike conventional cooling systems that require electricity and release waste heat to the environment. In recent years, RC technologies have advanced rapidly, moving steadily toward practical implementation and commercialization. Here, this mega-review offers a comprehensive overview of RC, encompassing its fundamental background, the underlying photonic and thermal principles, and fabrication approaches for constructing efficient cooling devices. We discuss a variety of RC structures along with their design strategies and explore the diverse functionalities that adapt RC toward particular requirements. We further review emerging applications of RC, highlighting practical implementations. Finally, we outline the key challenges and future directions, offering perspectives and insights to guide continued progress in this rapidly advancing field.

KEYWORDS: radiative cooling, thermal radiation, photonic materials, metamaterials, thermal management, energy efficiency, sustainable technologies



1. INTRODUCTION

Harit Keawmuang and Junsuk Rho

The accelerating pace of urbanization and global warming has led to an unprecedented rise in global cooling demand.¹ Cooling is no longer a luxury but a necessity for health, productivity, and comfort in many regions of the world, with the urban population projected to reach 66% of the world's total by 2050,² while cooling energy demand for air conditioning is expected to increase by 750% over the same period.³ Conventional air conditioning requires large amounts of electricity, necessitating major expansions in energy infrastructure. It also drives significant carbon emissions, and the refrigerants it uses have a high global warming potential that further worsens the climate burden.¹ Growing awareness of these energy and environmental challenges has stimulated interest in both improving conventional cooling systems and developing alternatives.

Radiative cooling (RC) has emerged as one of the most promising alternatives. It is a passive process in which a hot

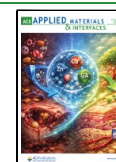
object loses heat by emitting thermal radiation toward a colder environment.^{4–6} Through this photon exchange, both energy and entropy are carried away, allowing the object to cool without external energy input, unlike conventional systems that consume electricity and release waste heat into the environment.⁷ However, the process requires coupling to a colder heat sink that can absorb the emitted radiation. RC is a process that occurs naturally in daily life. For instance, the human body, being warmer than its surroundings, continually releases heat to the environment through thermal radiation. On a larger scale, Earth

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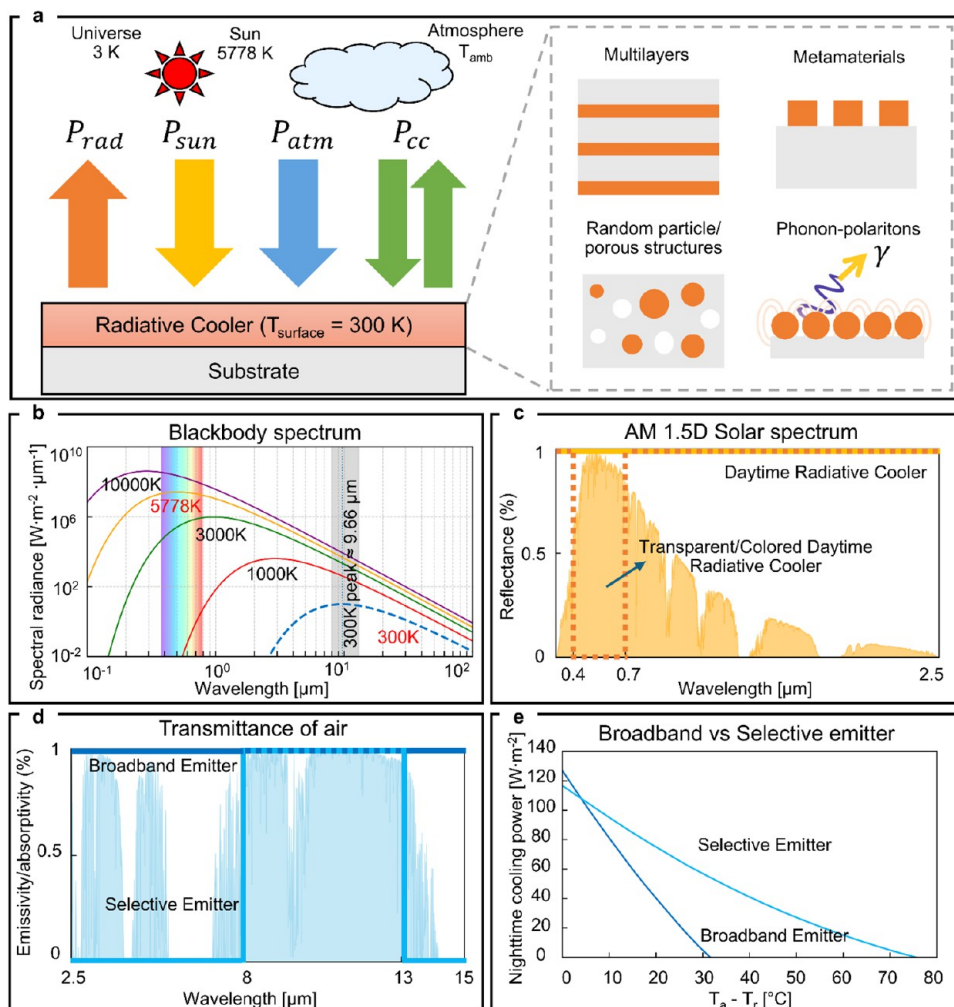


Figure 1. Principle and performance of radiative cooling systems. (a) Schematic illustration of the radiative cooling process, where the device exchanges heat with the universe (3 K), the Sun (5778 K), and the ambient atmosphere. The radiative cooler is typically realized through multilayers, metamaterials, random particle/porous structures, or phonon-polariton-based designs. (b) Blackbody radiation spectra at various temperatures with the 300 K emission highlighted, showing the overlap with the atmospheric window (AW). (c) Solar irradiance spectrum (AM 1.5D, 0.3–2.5 μm , orange shaded area) indicating the spectral range relevant for daytime radiative cooling, including transparent or colored radiative coolers. When the Sun is directly overhead (90° solar altitude), the air mass (AM) is defined as AM 1.0. At oblique incidence, sunlight passes through a thicker atmospheric path, resulting in higher AM values. AM1.5 is the most widely used standard condition on the ground (corresponding to latitudes of approximately $30\text{--}40^\circ$). Standard AM1.5D data set (ASTM G173) was normalized to their maximum value (set to 1) in order to compare the relative magnitudes across wavelengths. (d) Comparison of air transmittance (2.5–15 μm , blue shaded area) with broadband and selective emitters, emphasizing the importance of matching emissivity with the AW. (e) Nighttime cooling power as a function of temperature difference between the atmosphere and the cooler ($T_{\text{amb}} - T_{\text{surface}}$), comparing the performance of selective and broadband emitters. Reproduced with permission from ref 42. Available under a CC-BY 4.0 license. Copyright 2020 The Author(s).

(about 300 K) continuously radiates heat to the cold universe, which is at about 3 K, through the mid-infrared atmospheric window (8–13 μm).⁸ This spectral range coincides with the peak thermal emission of objects near ambient temperature, allowing a substantial portion of Earth's heat to escape directly into outer space, which effectively acts as the ultimate heat sink.^{9,10} Through this concept, a technology known as nighttime RC has been realized, in which a black emitter exposed to the sky radiates its internal heat to the cold universe and cools below the ambient temperature.^{11–16} Although RC occurs naturally, its practical implementation requires careful design and control. This becomes especially critical during the daytime, when the greatest cooling demand arises and the challenge is to achieve cooling even under direct solar irradiation. Traditional black emitters used in nighttime studies are ineffective in this case, as

they readily absorb sunlight and heat up instead of providing cooling.

Daytime RC addresses the limitation by employing spectrally selective structures that minimize absorption of solar radiation in the range $0.3 \leq \lambda \leq 2.5 \mu\text{m}$ while maintaining strong thermal emission in the mid-infrared atmospheric window.^{17–23} This spectral selectivity allows radiative coolers to function not only at night but also under direct sunlight during the day. The first demonstration of daytime RC is reported in 2014 by Raman et al.,²⁴ they use a multilayer photonic structure that reflects incoming solar radiation while emitting strongly in the atmospheric window. Following this breakthrough, the field of RC has rapidly advanced, with the development of diverse structural designs,²⁵ the expansion of key functionalities,^{26–31} and the emergence of a wide range of applications,^{32–38}

establishing it as a leading direction in energy-efficient technologies.

This mega-review presents a comprehensive overview of RC, covering its background, principles, structures, functionalities, and applications. We begin by introducing the fundamental photonic and thermal concepts that govern RC, and representative fabrication strategies for realizing radiative coolers. We then explore diverse structural configurations of radiative coolers, along with their design strategies and essential characteristics. Next, we highlight the key functionalities that tailor RC performance for specific needs, with a focus on physical principles, design approaches, and key performance metrics. Then, we further survey emerging applications across diverse domains, such as energy-efficient buildings, solar energy systems, and electricity generation, highlighting practical implementations of RC across these fields. Particular emphasis is placed on system-level performance, integration strategies, and real-world impact. Lastly, we discuss the remaining challenges and future outlook, aiming to offer both a broad perspective and useful insights for further development in this rapidly evolving field.

2. FUNDAMENTALS AND PRINCIPLES OF RC

2.1. Thermal Balance of RC

Junkyeong Park and Junsuk Rho

Heat transport originates from the nonequilibrium energy distributions of four fundamental carriers: phonons, electrons, fluid particles, and photons.^{6,39} Microscopic heat transfer phenomena can thus be interpreted through the behavior of these fundamental carriers. Phonons, representing quantized lattice vibrations, are responsible for thermal conduction in dielectric materials. Electrons contribute to thermal conduction particularly in conductors and semiconductors, where their concentration may be constant or vary with temperature. Fluid particles, whether monatomic or polyatomic, transfer heat through collisions with neighboring fluid particles, a process known as convection. Photons, the only carriers capable of transporting energy across a vacuum, span a broad energy range relevant to heat transport, from far-infrared to ultraviolet (UV). They interact with electric and magnetic entities, thereby defining material-specific electromagnetic responses. In general, heat transfer occurs through the transport of these carriers, whereas energy conversion arises from their inelastic interactions.

To examine photons in more detail, a photon can be interpreted not only as a particle but also as an electromagnetic wave. A blackbody is an idealized emitter that radiates electromagnetic energy solely as a function of its temperature. By introducing the concepts of quantized radiation energy and the Planck constant, Max Planck formulated the spectral distribution of blackbody radiation and demonstrated that the peak emission wavelength shifts with temperature (Figure 1b). The equation of this principle is as follows:⁹

$$I_{\text{BB}}(\lambda, T) = \frac{2hc^2}{\lambda^5} \frac{1}{e^{hc/\lambda k_B T} - 1} \quad (1)$$

where $h = 6.626 \times 10^{-34}$ Js is Planck's constant, $k_B = 1.381 \times 10^{-23}$ J/K is the Boltzmann constant, $c = 2.998 \times 10^8$ m/s is the speed of light. In this sense, every object at a temperature above 0 K continuously radiates thermal energy into its surroundings.

Radiative cooling technologies aim to enhance and control this naturally occurring process for efficient thermal manage-

ment. The Sun, at a temperature of around 5778 K, emits predominantly in the visible (VIS) range (Figure 1c), whereas the Earth, at approximately 300 K, emits primarily in the mid-infrared, particularly within 8–13 μm . Importantly, at the same time, Earth's atmosphere exhibits selective transparency in this range (Figure 1d). While water vapor strongly absorbs radiation below 8 μm and both water vapor and CO_2 absorb above 13 μm , the 8–13 μm region, known as the "atmospheric window (AW)", allows infrared radiation to escape into outer space with minimal absorption. This spectral overlap between terrestrial blackbody emission and the AW forms the physical basis of passive radiative cooling.

To describe the thermal behavior of a radiative cooler at the macroscopic level, heat transfer is governed by the heat flux P , which includes contributions from conduction, convection, and radiation (Figure 1a). These mechanisms are generally treated under the assumption of local thermodynamic equilibrium, where thermal energy is stored and exchanged in a quasi-static manner. Based on this framework, the net thermal behavior of a radiative cooling system can be expressed as⁴

$$P_{\text{cool}}(T, T_{\text{amb}}) = P_{\text{rad}}(T) - P_{\text{sun}} - P_{\text{atm}}(T_{\text{amb}}) - P_{\text{cc}}(T, T_{\text{amb}}) \quad (2)$$

Here, P_{cool} denotes the total cooling power of the system. P_{rad} is the thermal radiation emitted by the cooler, P_{sun} is the absorbed solar power, P_{atm} is the downwelling atmospheric thermal radiation absorbed by the cooler, and P_{cc} accounts for nonradiative energy exchange via conduction and convection. These terms are expressed as follows:

$$P_{\text{rad}}(T) = \int d\Omega \cos \theta \int_0^\infty d\lambda I_{\text{BB}}(T, \lambda) \epsilon(\lambda, \theta) \quad (3)$$

$$P_{\text{sun}} = \int_0^\infty d\lambda I_{\text{sun}}(\lambda) \epsilon(\lambda, \theta_{\text{sun}}) \quad (4)$$

$$P_{\text{atm}}(T_{\text{amb}}) = \int d\Omega \cos \theta \int_0^\infty d\lambda I_{\text{BB}}(T_{\text{amb}}, \lambda) \epsilon_{\text{atm}}(\lambda, \theta) \epsilon(\lambda, \theta) \quad (5)$$

The solid angle integral $\int d\Omega$ spans the hemisphere above the surface, and θ denotes the zenith angle. I_{BB} refers to the spectral radiance ($\text{W m}^{-2} \text{sr}^{-1} \mu\text{m}^{-1}$) of a blackbody. I_{sun} refers to the spectral irradiance ($\text{W m}^{-2} \mu\text{m}^{-1}$) of the sun, assuming that the structure is facing the sun at a fixed angle θ_{sun} . For I_{sun} , the AM1.5 solar spectrum ($I_{\text{AM1.5}}$) is commonly used as the standard terrestrial condition. $\epsilon(\lambda, \theta)$ is the directional spectral emissivity of the cooler, and $\epsilon_{\text{atm}}(\lambda, \theta)$ describes the angular and spectral dependence of atmospheric emissivity. The latter can be related to the zenith-direction transmittance (λ) through:

$$\epsilon_{\text{atm}}(\lambda, \theta) = 1 - \tau(\lambda)^{1/\cos \theta} \quad (6)$$

Finally, nonradiative heat exchange with the ambient environment is modeled as

$$P_{\text{cc}}(T, T_{\text{amb}}) = h_{\text{cc}}(T_{\text{amb}} - T) \quad (7)$$

where h_{cc} is an effective heat transfer coefficient encompassing both convective and conductive contributions.

For applications that demand cooling power either close to the ambient temperature or significantly below it, the emissivity of the radiative cooling surface can be tuned in various ways.^{4,40} A representative comparison can be made between a broadband emitter, which exhibits high emissivity over all infrared

wavelengths, and a selective emitter, which exhibits high emissivity only within the AW (Figure 1d). A broadband emitter enables large cooling power output. However, based on Kirchhoff's law, such a surface not only emits thermal radiation through the AW but also absorbs incoming radiation outside this range. This reciprocal effect limits its ability to reach temperatures lower than the ambient environment. In contrast, a selective emitter, characterized by near-unity emissivity solely within the AW, reduces absorption of downward atmospheric radiation and thereby enables deeper subambient cooling. Consequently, broadband emitters are advantageous for maximizing cooling power when the device temperature is above or near ambient, whereas selective emitters are better suited for achieving significantly lower surface temperatures. As illustrated in Figure 1e, the selective design reaches substantially lower equilibrium temperatures. The calculation assumes an ambient temperature of 27.15 °C under ideal conditions, with solar absorption and parasitic nonradiative losses neglected, and an atmospheric transmission spectrum corresponding to 60% relative humidity.

Additionally, the angular dependence of atmospheric emissivity can also be considered in cooler design to minimize P_{atm} . Atmospheric emissivity is highest at grazing angles ($\theta = 90^\circ$) within the 4–20 μm range, but lowest at normal incidence ($\theta = 0^\circ$) in the 8–13 μm window. Thus, tailoring the cooler's emissivity profile to account for angular variations in atmospheric radiation enhances its performance.^{4,40,41}

2.2. Photonic Concepts of RC

Junkyeong Park and Junsuk Rho

Nighttime radiative cooling,^{43,44} which enables thermal emission into outer space, has been studied and utilized since the 1970s. For decades, radiative cooling during the daytime was considered impossible because the solar radiation term (P_{sun}) is overwhelmingly large. However, in 2014, the concept of daytime radiative cooling^{23,45} was introduced, demonstrating that radiative cooling can also be achieved under direct sunlight. This is made possible by employing photonic structures capable of reflecting both visible and near-infrared (NIR) radiation. The key to daytime RC lies in minimizing solar absorption while maximizing thermal emission within the AW.

Recent progress in nanophotonics has enabled precise manipulation of electromagnetic properties using engineered nano- and microscale structures.⁹ Photonic structures of radiative coolers reported to date can be broadly classified into four categories: multilayer structures, metamaterials, random particles, and porous structures. Multilayer designs consist of stacked materials with carefully tuned sequences and thicknesses to achieve desired spectral responses. For example, dielectric-metal-dielectric layers can induce surface plasmon effects,⁴⁶ whereas alternating dielectric layers form Bragg mirrors;⁴⁷ both structures can be utilized to achieve reflection. Metal-dielectric-metal layers are often employed to design absorbers or emitters.⁴⁸ Metamaterials, composed of subwavelength structures, allow fine control of light-matter interactions, including the excitation of resonances and the creation of effective gradient refractive indices.^{49–51} By employing the photonic concepts of these structures, various radiative cooler designs that are transparent, colored, or tunable have also been proposed (dashed region in Figure 1c).

For practical deployment, scalability, cost-effectiveness, and optical robustness are critical. Unlike periodic designs, random particle and porous structures exploit multiple scattering in

disordered configurations to yield inherently broadband, polarization-independent, and angle-insensitive optical responses.⁵² Such characteristics are advantageous under incoherent and broadband illumination, for example, solar radiation. These structures can be fabricated from dielectric or metallic materials through scalable and low-cost techniques, including coating,⁵³ casting,⁵⁴ and spraying.⁵⁵ Collectively, these attributes constitute a practical platform that combines spectral control, manufacturability, and durability for large-scale radiative cooling applications.

The choice of materials is primarily determined by refractive index and absorption characteristics within the AW. High index materials such as titanium dioxide (TiO_2) and silicon (Si), low index materials such as polytetrafluoroethylene (PTFE) and silicon dioxide (SiO_2), are commonly employed. Materials such as polydimethylsiloxane (PDMS) and silicon nitride (Si_3N_4) exhibit strong phonon-polariton resonances within the 8–13 μm AW, enabling efficient thermal absorption in this spectral range. According to Kirchhoff's law of thermal radiation, their high absorptivity directly translates into high emissivity, making them effective radiative cooling materials. Since they are transparent in the visible range, their spectral properties can also be tailored for use as coatings in transparent or colored radiative cooling devices.^{28,56,57}

Metals such as silver (Ag) and aluminum (Al) exhibit high reflectivity and are widely used as underlying substrates or back reflectors in radiative cooling devices to suppress solar absorption and enhance cooling performance. Furthermore, by tailoring the metal layer thickness or nanostructure, plasmonic resonances can be engineered to enable selective transmission at desired wavelengths, produce desired colors, or tailor spectral absorption and therefore emissivity.

Biomimetic approaches have also been investigated, drawing inspiration from desert beetles,^{58,59} butterfly wings,⁶⁰ and plant cuticles^{61,62} to enhance radiative cooling. These structures provide passive thermal regulation, multifunctionality, and hierarchical ordering, improving solar reflectance and mid-infrared emissivity while ensuring scalability and environmental compatibility. Extending these principles to wearable devices, textiles have recently been proposed as a pathway for personal thermal management.^{32,63} Detailed examples and material-specific discussions will be presented in the following section.

2.3. Representative Fabrication Strategies

Heon Lee

The first passive daytime radiative cooling device was fabricated by vacuum-depositing a thin metallic silver film on a silicon wafer substrate to reflect incident solar radiation, and then repeatedly depositing thin films of silicon oxide and hafnium oxide with varying thicknesses to emit (absorb) infrared radiation in the atmospheric window region. This experiment was the first to experimentally demonstrate cooling below ambient temperature during the day via radiative cooling.²⁴ Subsequently, extensive research has focused on implementing selective emissions in the atmospheric window. Hossain et al. maximized selective emission in the window region using a photonic structure containing multilayer metamaterials of chromium and aluminum.⁴⁹ Zou et al. enhanced atmospheric window emissivity by forming a periodic metasurface structure using phosphorus-doped n-type silicon and silver.⁶⁴ Sequential deposition of different kinds of ceramic thin films also significantly increases infrared emission in the atmospheric window. Chae et al. fabricated a radiative cooling

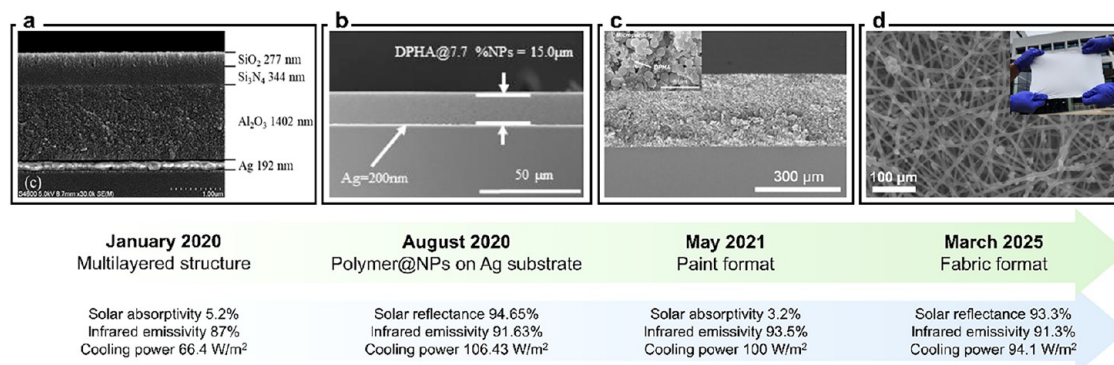


Figure 2. Evolution and performance progression of radiative cooling devices. (a) Multilayered thin film structure (January 2020). Adapted with permission from ref 22. Copyright 2020 American Chemical Society. (b) Dispersed nanoparticles in polymer matrix of Ag thin film (August 2020). Adapted with permission from ref 53. Copyright 2020 Elsevier. (c) Dispersed nanoparticles in polymer matrix (paint format, May 2021). Adapted with permission from ref 66. Copyright 2021 Elsevier. (d) Dispersed nanoparticles in polymer fiber (fabric format, March 2025). Adapted with permission from ref 67. Copyright 2025 Elsevier. The timeline and annotations summarize the reported optical/thermal performance for each generation, including solar absorptivity/reflectance, infrared emissivity, and cooling performance, to highlight performance improvements across successive device formats.

device by depositing aluminum oxide, silicon nitride, and silicon oxide at thicknesses of 1402, 344, and 277 nm, respectively, achieving a solar absorption rate of 5.2% and atmospheric window emissivity of 87%.²² Ma et al. improved atmospheric window emission by multiple-layer deposition of silicon oxide and silicon nitride, excluding alumina, and used a silver thin film for solar reflection.⁶⁵ However, multilayer ceramic film composition is not always effective, facing disadvantages such as high processing cost and restrictions on substrate types due to high temperature processes.

Dispersing ceramic microparticles in a polymer matrix can boost emissivity in the window region through the covalent bonds of the polymer and the resonant infrared absorption of the ceramic particles, potentially replacing multilayer ceramic thin films. Forming a polymer layer with dispersed ceramic microparticles over a silver thin film results in a simpler radiative cooling device. Professor Yin at the University of Colorado developed an advanced radiative cooling material by dispersing silica microparticles in a polymethylpentene (TPX) polymer.⁵² Professor Lee's research group at Korea University mixed alumina, silica, and silicon nitride—previously thin-film materials—in particle form into dipentaerythritol penta-hexaacrylate (DPHA) polymer and coated it on a silver layer to implement a radiative cooling device.⁵³ However, this method makes it difficult to achieve selective high emissivity only in the atmospheric window; instead, it achieves high reflectance across the entire long-wave infrared region, including the window (Figure 2).

A method to achieve over 96% solar reflectance without using metallic silver was proposed. Son et al. secured high reflectance across all solar wavelengths by employing microscopic pore scattering formed from blends of different polymer matrices, instead of mirror reflection with silver films. Using poly(vinylidene fluoride) (PVDF) powder and polyurethane acrylate (PUA), they achieved 93% solar reflectance and 93% average atmospheric window emissivity.⁶⁸ Yet, such methods have drawbacks: the polymer matrices are expensive, and the presence of micropores can compromise device durability. Alternatively, ceramic particles with high whiteness, reflectance, and refractive index—capable of strong solar scattering—are dispersed in more common polymer matrices for radiative cooling devices. Barium sulfate and calcium carbonate particles

were first explored, leading to the development of paint-type radiative cooling devices. Professor Ruan at Purdue University published a white paint using BaSO₄ and an acrylic binder, showing excellent cooling performance with 97.6% solar reflectance and 96% atmospheric window emissivity.⁶⁹ The research group also created a device utilizing CaCO₃ particles, achieving 95.5% solar reflectance and 94% window emissivity.⁷⁰ Subsequently, research utilizing various ceramic particles or combinations of particles has been actively conducted.^{23,66,71,72} These paint-type radiative cooling devices are a form where ceramic particles are dispersed in a liquid polymer resin. When applied as a paint film on various substrates, this film reflects the incident sunlight by scattering with ceramic particles, while the polymer resin and dispersed ceramic particles within the coating show high absorption for long-wavelength infrared, including the atmospheric window region, thereby enabling radiative cooling. Compared to conventional paint, which maxes out at 88% solar reflectance, the high incident solar reflectance of over 96% makes it possible for radiative cooling to achieve temperatures lower than the ambient temperature even during the sunny daytime. Paint-type radiative cooling devices offer lower manufacturing costs by using inexpensive ceramic particles with no degradation from silver oxidation, high versatility as coatings can be directly applied to metals, resins, concrete, wood, and more, and direct applicability to large-area objects. Despite these advantages, practical deployment of paint-type RC devices still faces several challenges. One of the primary concerns is the long-term outdoor durability. Among these, soiling can reduce solar reflectance over time by depositing contaminants on the coating surface.^{33,73} In this regard, hydrophobic or self-cleaning RC designs^{73–76} that can withstand physical cleaning are promising for mitigating soiling, maintaining cooling performance, and extending operational lifetime. Furthermore, prolonged exposure to solar UV irradiation can gradually degrade RC performance over time.⁷⁷ To mitigate this issue, fluoropolymer-based coatings can be integrated into RC systems, as their relatively low UV absorption helps preserve solar reflectance, hence preserving long-term outdoor stability.⁷⁸ Adhesion to different substrates is another important practical consideration for paint-type RC systems, particularly for architectural coating applications, as insufficient interfacial stability can lead to peeling, cracking, or delamination

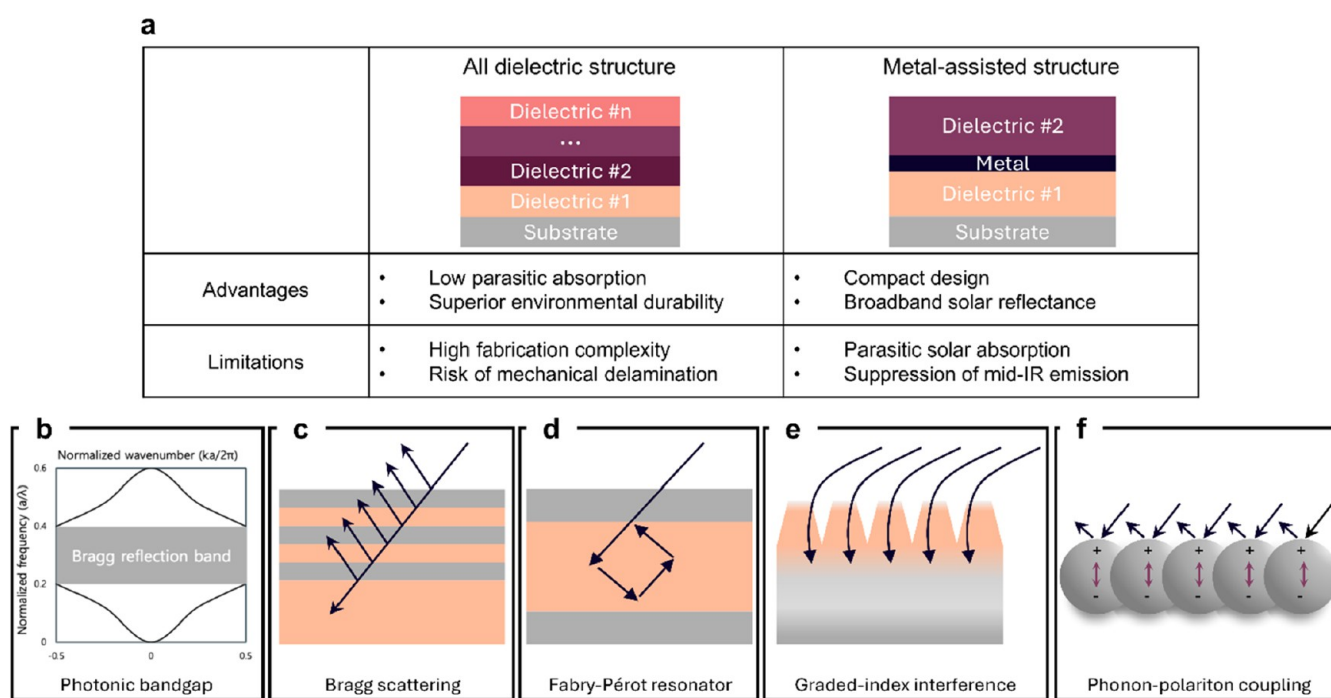


Figure 3. An overview of multilayer designs and their physical mechanisms for radiative cooling. (a) Comparative summary of all-dielectric multilayer structures and metal-assisted structures. (b) Photonic bandgap in a 1D photonic crystal. (c) Bragg scattering and interference effects. (d) Fabry–Pérot resonance between two reflective surfaces. (e) Interference in a graded refractive index. (f) Phonon-polariton resonance.

during long-term outdoor use.⁷⁹ Accordingly, recent RC coating designs have increasingly sought to improve substrate adhesion together with outdoor durability and optical performance.^{80,81}

Another form is radiative cooling fabrics. By incorporating ceramic nanoparticles during polymer fiber fabrication, fibers embedded with these particles can be woven into fabrics with radiative cooling properties (i.e., high solar reflectance and high atmospheric window emissivity). A simpler method is to create fabric using electrospinning by mixing ceramic nanoparticles such as TiO₂ and Al₂O₃ into polymer resins like PU, PAN, or PVDF.^{82,83} Subsequently, treatments such as pressing can be applied to ensure the fabric has appropriate mechanical properties, thereby producing a fabric with radiative cooling function.⁸⁴ Textile-form radiative cooling materials have great industrial and economic potential because they can be used directly in clothing and hats to enhance thermal comfort. Iqbal et al. embedded ZnO in a polyethylene matrix to fabricate textiles by electrospinning, yielding personal thermal management material that reflects sunlight while allowing body heat emission.³⁸ Park et al. reported electrospun fibers with excellent radiative cooling performance, based on PMMA, thermoplastic polyurethane (TPU), and Al₂O₃ nanoparticles.⁸⁵ However, the ceramic nanoparticles and nanopores added to realize the radiative cooling function can potentially impair the inherent properties of the fabric. For example, deterioration in the fabric's mechanical strength, flexibility, wrinkle recovery, and texture are typical problems. Various researchers are working on producing fabrics with excellent radiative cooling ability while minimizing these problems. For instance, Lim et al. developed a fabric-type cover sheet using PU and TiO₂ materials via an electrospinning process, and their research team confirmed that the mechanical strength and optical properties were maintained even after over 1000 cycles of tension and contraction.⁶⁷

3. STRUCTURES OF RC

3.1. Multilayer Thin Film Structures

Seokju Choi and Sunae So

Multilayer thin films, composed of alternating layers of materials with distinct optical properties, are among the earliest and most extensively investigated approaches for RC (Figure 3a). Their primary function is to suppress solar energy absorption while simultaneously enhancing thermal emission within the atmospheric transparency window. This dual spectral control is governed by well-established photonic mechanisms, including photonic bandgaps⁸⁶ arising from Bragg scattering,⁸⁷ Fabry–Pérot resonances,⁸⁸ graded-index interference⁸⁹ and, in some cases, phonon-polariton coupling⁹⁰ (Figure 3b–f). Owing to their rigorous theoretical foundation, compatibility with mature thin-film fabrication methods, and adaptability across a wide range of substrates, multilayer thin films continue to serve both as benchmark systems and as practical platforms for scalable RC.

The operating principles of multilayer structures are rooted in classical optics. Periodic stacks of high- and low-refractive-index materials generate Bragg scattering and associated photonic bandgaps, where light propagation is strongly suppressed. When aligned with the solar spectrum (0.3–2.5 μm), such bandgaps enable broadband reflection, thereby effectively minimizing parasitic solar heating.^{22,24} Fabry–Pérot resonances provide another route to spectral control:^{91–94} placing a dielectric spacer between two reflective interfaces creates standing-wave modes that selectively enhance emissivity in the mid-infrared. By adjusting cavity thickness, these emissivity peaks can be positioned within the atmospheric window (8–13 μm), allowing for efficient thermal emission. Beyond such discrete mechanisms, graded-index multilayer structures,^{45,95,96} where refractive index or layer thickness changes gradually across the stack, produce broadened reflection bands. In practice, high-

performance multilayer films typically combine multiple mechanisms, often supplemented by the intrinsic vibrational resonances of the chosen materials.

Materials are central to performance. Transparent dielectric oxides such as SiO_2 , TiO_2 , HfO_2 , Al_2O_3 , and ZrO_2 are widely employed due to their generally low optical losses across most of the solar spectrum and good thermal stability, making them ideal for alternating high/low-index layers in Bragg-type designs. Low-index fluorides such as MgF_2 and CaF_2 further increase refractive index contrast, thereby strengthening interference effects in the solar band. These fully dielectric multilayers can achieve excellent solar reflectance and robust mid-infrared emissivity, though typically at the expense of requiring many layers, increasing fabrication complexity.

Incorporating metals into multilayer structures offers a more compact route to broadband solar reflection. Metal-assisted multilayer designs take several forms, including metal-backed dielectric stacks,²⁴ dielectric-metal-dielectric (DMD) structures^{97,98} and hyperbolic metamaterials (HMMs).^{99,100} DMD stacks place a thin metal film between dielectric layers, providing broadband reflection across the solar spectrum with only a few layers, while the dielectrics tune interference effects and protect the metal surface. Metal-backed dielectric stacks adopt a simpler geometry in which a reflective metal substrate serves as the bottom mirror upon which dielectric multilayers are deposited to tailor mid-infrared emission. HMMs, composed of deeply subwavelength alternating metal and dielectric layers, exploit extreme optical anisotropy to control spectral response across distinct wavelength bands. Despite these structural advantages, metallic layers paradoxically introduce several practical limitations that compromise their overall performance and longevity. They introduce parasitic absorption, converting a fraction of incident sunlight into heat. In addition, metals generally exhibit low intrinsic emissivity in the mid-infrared, meaning that efficient thermal emission must be achieved through careful design of the surrounding dielectric or resonant structures. A common workaround has been to add an emissive polymer overlayer, which restores emission in the mid-infrared.^{101,102} However, these polymers complicate fabrication workflows by requiring separate processing routes (e.g., spin coating or dip coating) that are not directly compatible with vacuum-based thin-film deposition. Furthermore, polymers degrade under long-term UV exposure, leading to yellowing, cracking, or reduced emissivity, ultimately shortening device lifetime.¹⁰³ Thus, while metal-assisted multilayers remain attractive for transparent RC applications such as smart windows, their reliance on metals continues to impose fundamental limitations.

An alternative approach involves incorporating polar dielectrics such as SiC , SiO_2 , and BaSO_4 into multilayer stacks. These materials support phonon–polariton resonances in the mid-infrared, producing selective emissivity peaks that naturally align with the atmospheric window. By coupling interference effects with vibrational resonances, such multilayers achieve strong thermal emission without relying on polymers or suffering from metallic absorption losses.

Fabrication of multilayer films leverages well-established thin-film deposition techniques. Physical vapor deposition, where a solid source material is physically converted into a vapor through processes such as evaporation such as evaporation^{24,104} and sputtering,¹⁰⁵ are most widely used offering nanometer-scale thickness control and high film uniformity.¹⁰⁶ Chemical vapor deposition, which involves introducing precursor gases that

chemically react or decompose on the substrate surface to form the desired film, is also used for dielectric layers, especially when low-temperature growth is required.^{107–110} Atomic layer deposition provides angstrom-level precision and excellent conformality, making it particularly attractive for hybrid or graded-index designs where exact layer control is critical. More recently, sol–gel processing^{111,112} and solution-based spin-coating¹¹³ have been explored as low-cost alternatives, though their reproducibility and precision are still limited. For practical deployment, industrial-scale methods such as roll-to-roll sputtering¹¹⁴ and glass-coating lines¹¹⁵ are promising, yet achieving defect-free interfaces and thickness precision across tens of alternating layers remains a formidable technical challenge.

Despite significant progress, multilayer thin films present ongoing design and fabrication challenges. Fabrication can be complex and costly, especially when many alternating layers are required to achieve broadband reflectivity. This can increase manufacturing time and may lead to mechanical stress within the film, potentially causing delamination.¹¹⁶ Interference-based optical responses are inherently angle-dependent, reducing cooling effectiveness under diffuse or oblique sunlight. Additionally, there are material constraints: high-refractive-index dielectrics that are both perfectly nonabsorbing across the entire solar spectrum and stable under environmental conditions are scarce. Finally, while thin-film deposition is scalable in principle, achieving large-area, defect-free multilayer structures with precise thickness control across many layers remains a bottleneck for mass production.

Looking forward, several research directions appear especially critical. Improving angular robustness through graded-index designs^{117–119} will be crucial for stable performance under realistic outdoor conditions. Enhancing durability by replacing polymer overlayers with inorganic emissive coatings,^{120,121} or by employing alloyed¹²² and encapsulated^{120,123,124} metallic films, could significantly extend device lifetimes. At the same time, discovering or engineering new dielectric compounds with tailored refractive indices would expand the design space beyond the relatively narrow set of oxides and fluorides currently available.^{125–127} The integration of polar dielectrics is particularly attractive, as their intrinsic phonon–polariton resonances align naturally with the atmospheric window, offering selective emissivity without reliance on metals or polymers.^{128–131} Employing scalable fabrication strategies are also important. Hybrid approaches that combine precision thin-film layers with solution-based or roll-to-roll coatings may offer a path toward affordable large-area deployment.^{56,132,133} Finally, computational optimization techniques and AI-driven inverse design are expected to further accelerate progress, as the optical response of multilayer films can be readily modeled.^{21,57,134} Leveraging such tools to achieve multiobjective, high-performance structures that not only maximize RC performance but also integrate additional functions such as durability, self-cleaning, and aesthetic control will open opportunities for multifunctional coatings with real-world relevance.^{27,135–137}

3.2. Metasurfaces and Nanophotonic Structures

Changhyeon Lim and Trevon Badloe

Metasurfaces are two-dimensional structures with precisely arranged subwavelength features that enable complete control of the optical properties of light.^{138,139} As the optical response of a metasurface can be finely tuned by adjusting the material and geometrical parameters of its constituent structures, known as

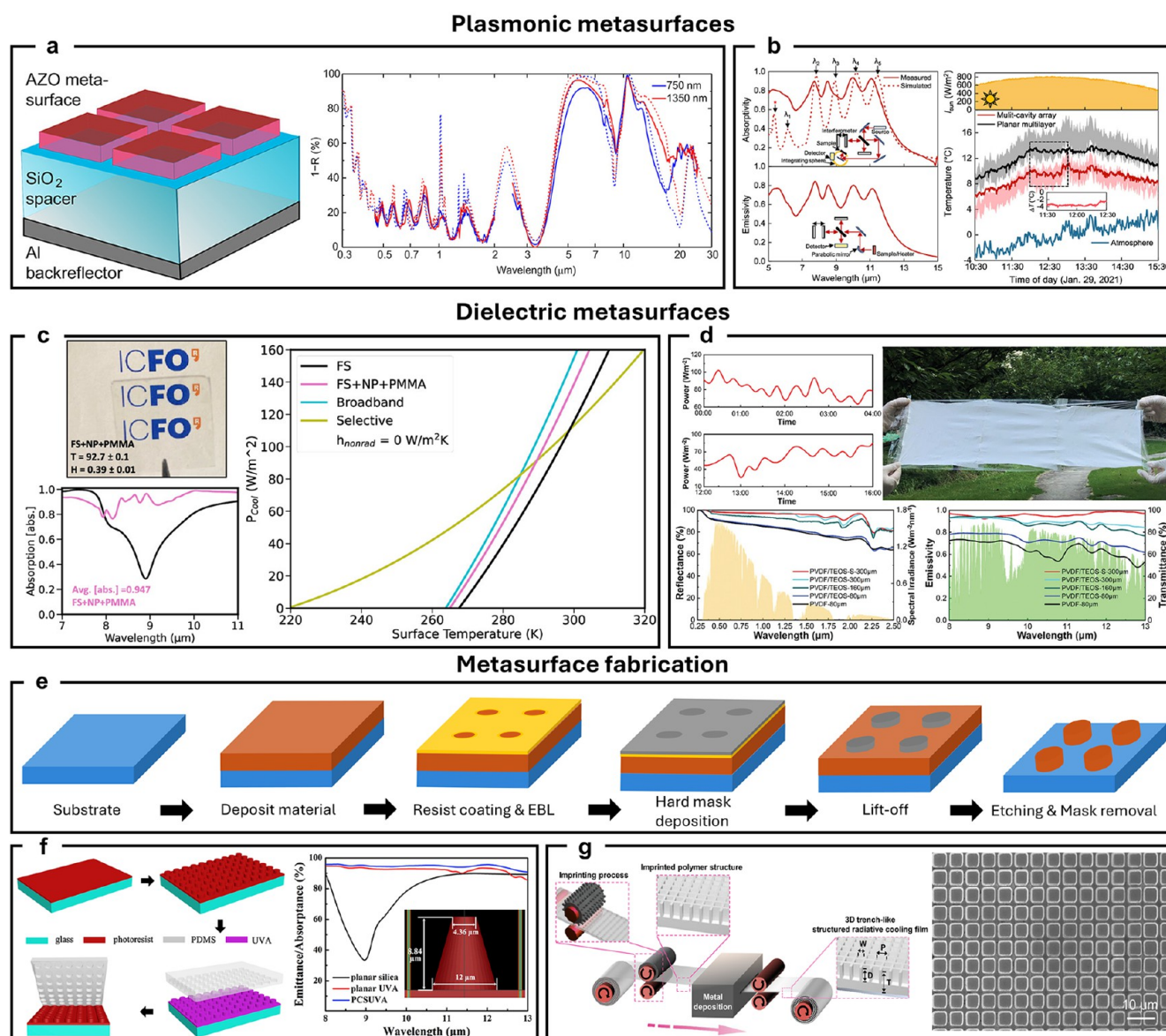


Figure 4. Metasurfaces and nanophotonic structures of RC. (a) Schematic cross-section of the metasurface-based radiative cooler for space applications (left) and measured absorption spectra (right). Adapted with permission from ref 144. Copyright 2018 American Chemical Society. (b) Absorption and emissivity spectra within the atmospheric window (left) and comparison of daytime cooling performance between planar and multicavity structures (right). Adapted with permission from ref 146. Copyright 2021 American Chemical Society. (c) Photos of transparent metasurface-based radiative cooler (top left) and absorption spectra (bottom left). Calculated cooling power (left). Adapted with permission from ref 147. Copyright 2022 American Chemical Society. (d) RC power throughout the day (top left) and large radiator pasted on a transparent membrane (top right). Reflectance and emissivity spectra in atmospheric window (bottom). Adapted with permission from ref 149. Copyright 2020 Wiley-VCH. (e) Schematic of a standard metasurface fabrication method. (f) Schematic of nanoimprint fabrication method (left) and simulated absorbance spectra (right). Adapted with permission from ref 157. Copyright 2019 Elsevier. (g) Schematic of the roll-to-roll nanofabrication process (left) and scanning electron microscope (SEM) image showing the uniform meta-atoms. Adapted with permission from ref 133. Copyright 2023 Springer Nature.

meta-atoms, they have shown extreme applicability for RC applications, where the manipulation of the absorption/emission across the spectrum from the visible to the mid-infrared region is required. This is generally designed through multipole resonances designed at specific locations through plasmonics or high refractive index dielectrics. With these versatile properties, metasurfaces have emerged as a powerful tool for managing thermal radiation and enabling daytime RC.^{9,40,140}

Since metasurfaces can be designed with resonance characteristics at specific wavelengths, they allow for direct implementa-

tion of efficient emission through the atmospheric window and simultaneous modulation of visible and NIR wavelengths, the keys for daytime RC. Plasmonic metasurfaces are engineered to modulate the spectral response through various mechanisms at metal/dielectric interfaces¹⁴¹ and have been proven for RC purposes.^{142,143} Sun et al. developed a metasurface-based optical solar reflector using aluminum-doped zinc oxide (AZO) as a transparent conductive oxide for the RC of spacecraft (Figure 4a).¹⁴⁴ The AZO is a plasmonic material in the infrared, while staying transparent in the visible, providing a high thermal emissivity of 79% in the infrared region and a low solar

absorptance of 16% in the visible range. Not only the optical performance of the AZO, but also its mechanical and thermal robustness prove it to be a strong choice for spacecraft solar reflectors. In space applications, however, the requirement for selective emission through the atmospheric window is relaxed, reducing one of the design requirements for metasurface-based daytime radiative coolers.

Gap plasmon resonances in metal–dielectric–metal cavities have been proposed as an effective strategy for RC due to their broadband thermal emission.¹⁴⁵ Cho et al. demonstrated a multicavity Cu/ZnS/Cu metasurface that supports multiple gap plasmon resonances, providing 62% emissivity in the atmospheric window (Figure 4b).¹⁴⁶ Experiments showed a substrate temperature reduction of up to 4 °C compared with a planar Cu/ZnS/Cu thin film. This highlights the potential of plasmonic metasurfaces in RC applications compared to simple multilayer structures. While the control of emission spectra with multiple plasmonic meta-atoms exhibiting low-Q resonances is a powerful answer to terrestrial- and space-based cooling applications, recently, there has been a rise in the use of all-dielectric materials for the creation of metasurfaces.

The main drawback of using metals in RC metasurfaces is the inherent absorption that they possess, which will reduce the efficiency of the device through Ohmic heating. Therefore, all-dielectric metasurfaces have been demonstrated as solutions to daytime RC.^{64,119} In one example, Arrés Chillón et al. proposed a lithography-free approach for RC using a transparent glass surface decorated with randomly distributed nanopillars in (Figure 4c).¹⁴⁷ The nanopillars are randomly distributed but approximating a periodic arrangement. The addition of the nanopillars suppresses the infrared reflection of SiO₂ at 9 μm, achieving a near unit emissivity. Furthermore, an additional PMMA polymer coating was applied to mitigate haze caused by the deep nanopillar structures in the visible spectrum by reducing the surface scattering. This resulted in a high transmittance of $T = 93.1\%$, producing a radiative cooler with a $P_{\text{cool}} = 138.74 \text{ W m}^{-2}$ while maintaining the transparency of glass.

When the wavelength of incident light is comparable to the geometric dimensions of the meta-atom, oscillations in the electromagnetic field are induced, leading to Mie scattering.¹⁴⁸ This scattering reduces solar absorption and can be harnessed for various RC applications. Wang et al. incorporated nanopores with diameters in the range of 100–200 nm into a flexible metasurface-based radiative cooler, inducing Mie scattering that resulted in a solar reflectance of 97% and an infrared emissivity of 96% (Figure 4d).¹⁴⁹ Experimental measurements demonstrated a daytime temperature reduction of up to 6 °C and a RC power of 61 W m^{-2} , while also exhibiting excellent flexibility and mechanical strength, indicating strong potential for large-scale practical deployment. While solar reflectance depends on the areal coverage ratio, cooling performance within the atmospheric window is most sensitive to geometric parameters such as pattern size, spacing, and shape.¹⁵⁰

The design of RC structures faces interesting photonic challenges due to the order of magnitude wavelength mismatch between the visible regime (100s of nanometers) and the mid-infrared (micrometers). This makes the design process a multiscale problem, which can be difficult to achieve heuristically; therefore, artificial intelligence (AI) has been implemented in the design and optimization process.¹⁵¹ Su et al. applied the k-nearest neighbor algorithm to construct regression models for optimizing the parameters of both quasi-periodic

metasurfaces and cross-trapezoidal cavity metasurfaces.¹⁵² The optimized configurations achieved high emissivity within the atmospheric window of 96.98 and 97.81%, respectively, while maintaining low solar absorptances of 9.34 and 7.21%, respectively. Under ambient conditions, these designs yielded net cooling powers of 63.48 and 90.13 W m^{-2} . Meanwhile, Ding et al. reported a biomimetic metasurface using AI-driven inverse design.¹⁵³ Three types of SiO₂-based photonic structures, truncated cones, cylinders, and cones were modeled with varying geometric parameters, and simulated data were used to train a generative deep learning model. The resulting inverse-designed truncated-cone arrays experimentally exhibited an average emissivity of 95% within the atmospheric window, 95% reflectance in the solar spectrum, and a cooling of 8.5 °C, all while maintaining robust manufacturability due to low aspect ratios. These AI-assisted inverse design schemes for metasurface-based RC show that the multiscale and multidimensional problems can be successfully solved through advanced computational methods that consider the materials and fabrication constraints directly into their optimization function.

After the metasurface-based radiative cooler has been designed, it should be physically realizable for real-world use. Generally, metasurfaces are fabricated using standard lithography techniques (Figure 4e), which gives them a huge advantage in terms of fabrication compared to three-dimensional metamaterials. However, the manufacturability of large-scale metasurfaces for RC is still one of the main challenges. Efficient modulation of the solar spectrum with meta-atoms requires precise nanoscale fabrication, which is in complete contrast with the physical size required for radiative coolers that should be at least centimeter, if not meter-scale in size, for any meaningful application. Electron beam lithography has been generally utilized to realize such nanometer resolution, as it offers a significantly shorter effective wavelength compared to conventional photolithography techniques (e.g., ArF, KrF).¹⁵⁴ Despite the resolution advantages of electron beam lithography, its low throughput and high operational costs remain significant limitations for large scale fabrication.

Nanoimprint lithography, which replicates patterned molds directly onto a substrate via physical contact, offers reduced fabrication costs and scalability for mass production of metasurfaces.^{155,156} Nanoimprint lithography has been used to fabricate truncated cone-shaped 2D photonic crystal structures of a UV-curable adhesive, serving as a versatile and large-area manufacturing method for high-resolution nanopattern transfer (Figure 4f).¹⁵⁷ The truncated cone geometry was produced via a photopolymerization reaction of the UV-curable resin. Subsequently, a composite structure comprising a polyethylene terephthalate substrate and Ag reflective layer was utilized to achieve thermal emission. The fabricated RC film exhibited an emissivity of 95% within the infrared atmospheric transparency window and achieved a maximum temperature reduction of $7.7 \pm 0.2 \text{ °C}$ in outdoor experiments. This fabrication method does not require high-temperature processing or chemical etching, enabling its facile application to flexible polymer substrates such as PET, allowing it to be adapted for various applications.

Recently, high-throughput nanoimprinting of large-scale metasurfaces has been demonstrated using roll-to-plate¹⁵⁸ and roll-to-roll (R2R) techniques. For RC, Lin et al. proposed a polymer-based metasurface through R2R nanoimprinting (Figure 4g).¹³³ After the R2R process, a physical vapor deposition process was followed to coat a 100 nm silver layer on the backside of the film to enhance the reflectivity. Owing to

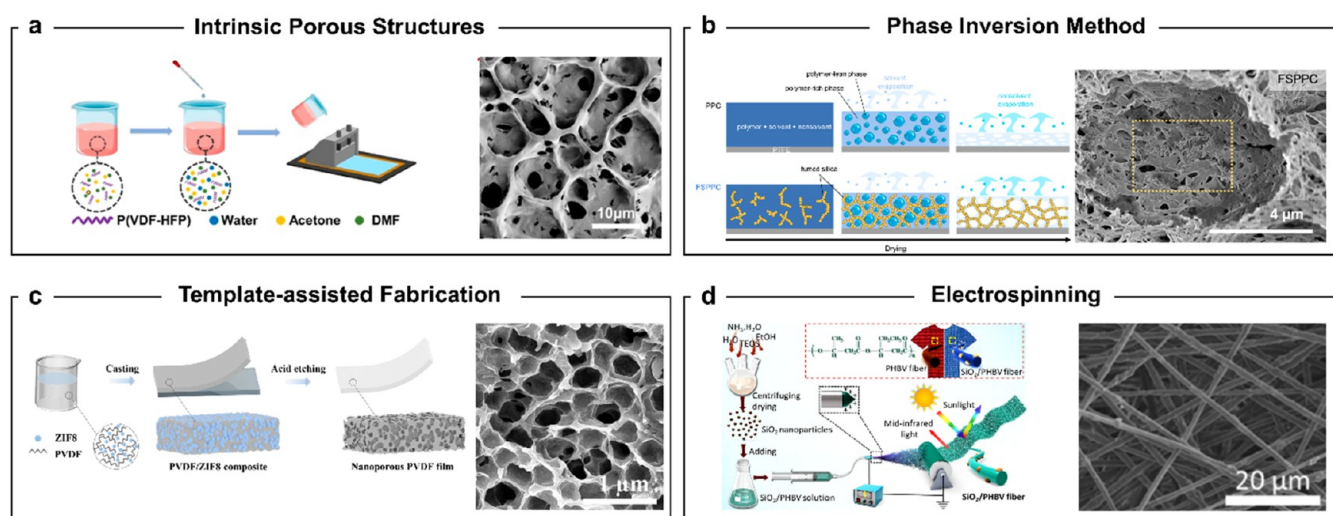


Figure 5. Representative fabrication routes for nanoporous radiative cooling materials. (a) Intrinsic porous PVDF–HFP films fabricated via a nonsolvent-induced phase separation (NIPS) process, showing the fabrication schematic and the resulting hierarchically interconnected porous structure of the optimized PVDF–HFP-5 film. Reproduced from ref 163. Copyright 2024 American Chemical Society. (b) Phase inversion via solvent–nonsolvent exchange, yielding asymmetric membranes with interconnected micropores and macrovoids, with SEM morphology highlighting their broadband scattering capability. Reproduced from ref 186. Available under a CC-BY 4.0 license. Copyright 2024 Author(s). (c) Fabrication process of a PVDF_{NP} film and a cross-sectional SEM view of the resulting structure, characterized by an average pore diameter of ~ 400 nm. Reproduced from ref 168. Copyright 2024 American Chemical Society. (d) Schematic of the preparation process for the Poly(3-hydroxybutyrate-co-3-hydroxyvalerate) (PHBV) and SiO₂/PHBV fiber membranes, with SEM image of SiO₂/PHBV fiber membranes 15 wt % SiO₂ concentrations. Reproduced from ref 209. Copyright 2025 American Chemical Society.

the flexibility of the polymer film, the metasurface-based radiative cooler exhibited a low solar absorptance of 4.8% and an excellent omnidirectional absorptance/emissivity of 96.1% in the atmospheric window. This continuous, large-area manufacturing approach is advantageous for practical applications and is expected to meet demanding requirements for metasurface-based RC performance in the future.

In summary, metasurfaces provide an attractive solution to RC due to their potential for multispectral manipulation through resonance engineering with metal and dielectric materials. However, due to the large disparity in wavelength scales between the visible and mid-infrared regimes, it is challenging to achieve ideal solar reflection and infrared emission simultaneously using a single material or a single pattern. Furthermore, the angular-dependent nature of standard metasurfaces limits full emission to the atmospheric window and could have a profound effect on the performance of metasurface-based radiative coolers. These limitations necessitate the adoption of complex designs such as multiscale architectures, multiple patterned layers, and combinations of hybrid material resonators,¹⁵⁹ while AI has been proven as a useful tool for photonic design and optimization. Recent research has increasingly focused on improving the durability and environmental stability of metasurfaces under diverse weather conditions, including high humidity, temperature fluctuations, and prolonged ultraviolet exposure,⁶³ as well as color-preserving radiative coolers for aesthetic outdoor purposes.⁵⁷ Such advancements are critical to ensuring long-term performance and reliability in real-world outdoor applications. Considering the unique advantages that metasurfaces offer, alongside the advancements in computational design and large-scale nanofabrication techniques, metasurface-based radiative coolers could still prove to be one of the go-to solutions for passive RC devices.

3.3. Porous Structures

Changhwan Hyeon, Minseo Jeong, and Dasol Lee

Nanoporous architectures have emerged as a promising and scalable platform for RC materials due to their ability to manipulate light–matter interactions through engineered multi-scale porosity.^{24,160} Within a single metal-free layer, broadband solar reflectance ($0.3\text{--}2.5\ \mu\text{m}$) and strong mid-infrared (MIR) emissivity ($8\text{--}13\ \mu\text{m}$) can be achieved without metallic back reflectors or complex multilayer stacks, provided that sufficient optical thickness, hierarchical nano-to-micro porosity, and optically nonabsorbing or highly reflective substrates are employed.¹⁶¹ These combined optical responses enable subambient operation with temperature drops up to $\sim 10\ ^\circ\text{C}$ under sunlight.¹³² Such passive cooling provides energy-free thermal management for applications ranging from wearable electronics to buildings and biomedical devices.¹⁶²

The cooling performance is governed by optical, structural, and material factors.¹⁶³ Based on Mie scattering principles, the peak scattering wavelength scales with the void diameter; submicron pores predominantly scatter UV and visible light, and micron-scale voids shift the scattering peak to extend scattering into the NIR.²⁰ Their hierarchical integration ensures uniformly high solar reflectance without spectral gaps.¹⁶⁴ High dielectric contrast between matrix and voids amplifies scattering, and interconnected pore architectures induce dependent scattering that broadens the resonance profile, while minimizing absorption reduces heat gain.¹³⁷ Structurally, porosity (60–90%) lowers effective refractive index and boosts MIR emissivity though excessive porosity weakens durability.¹⁶⁵ Pore connectivity, isotropy, and morphology also govern angular stability and can impart hydrophobicity or self-cleaning.¹⁶⁶ Materials must pair low solar absorption with strong MIR phonon–polariton resonances, as in fluoropolymers, cellulose, and ceramics, while resisting degradation for outdoor reliability.¹⁶⁷

The realization of these attributes depends critically on fabrication methodology, which determines pore morphology, size hierarchy, connectivity, and scalability. Several representa-

tive strategies have been widely adopted. Intrinsic porous structures, arising from natural morphologies or stress-induced voids in semicrystalline polymers, enable facile processing and low cost; however, they often require nonmetallic auxiliary reflectors, such as highly reflective substrates, dielectric backings, or white polymer supports, to compensate for limited scattering strength or insufficient layer thickness and thereby achieve high radiative cooling performance, rather than metallic mirror back reflectors.¹⁶⁸ Phase inversion, based on solvent–nonsolvent exchange, generates hierarchical porosity in polymers, yielding large-area coatings with high reflectance and emissivity.¹⁶⁹ Template-assisted methods use sacrificial particles to form tunable voids in poly(methyl methacrylate) (PMMA) or PDMS, while hard templates such as anodic aluminum oxide (AAO) membranes can guide ordered pore architectures with precise control.¹⁷⁰ Finally, electrospinning creates fibrous networks with nano/micropores, combining strong scattering with flexibility and textile-scale production.¹⁷¹

Here, we review these four fabrication routes, emphasizing processing–structure–property relationships that dictate optical performance, mechanical stability, and durability. We systematically compare intrinsic porous structures, phase inversion, template-assisted fabrication, and electrospinning, highlight recent advances, and propose guidelines for scalable RC materials in energy and healthcare.

3.3.1. Intrinsic Porous Structures. Intrinsic porous structures exploit the inherent crystalline morphology and deformation behavior of semicrystalline polymers to generate hierarchical porosity without sacrificial templates.¹⁷² In polyethylene (PE) and polypropylene (PP), crystalline lamellae and tie molecules act as stress concentrators where voids nucleate during stretching or controlled phase rearrangement. Cavitation under uniaxial or biaxial deformation produces micro- to mesoscale voids, while thermal or chemical modulation of lamellar spacing introduces nanopores.¹⁷³ This distribution—nanopores (<100 nm) for UV scattering, submicron pores (≈ 200 –800 nm) for visible backscattering, and micron-scale voids (≈ 1 –10 μm) for NIR reflection—enables broadband solar reflection.¹⁷⁴ Furthermore, vibrational resonances of the polymer backbone yield strong emissivity within the 8–13 μm atmospheric transparency window, a prerequisite for RC.¹⁷⁵

For instance, Li et al.¹⁶³ reported an intrinsically porous radiative cooling film based on PVDF–HFP, fabricated via a nonsolvent-induced phase separation (NIPS) process with rationally tuned solvent compositions. During solvent evaporation, spontaneous phase separation between polymer-rich and polymer-poor domains generated a hierarchically interconnected porous structure spanning nano- to microscale length regimes, as confirmed by scanning electron microscopy (SEM) (Figure 5a). By adjusting the solubility parameter mismatch between the polymer and mixed solvents, the pore size distribution and overall porosity were effectively controlled, enabling efficient broadband solar scattering. The optimized PVDF–HFP film exhibited a high solar reflectance of 97.7% and a mid-infrared (MIR) emissivity of 96.7%, without the use of any inorganic fillers or auxiliary reflective layers. As a result, the film achieved a subambient temperature reduction of approximately 5.4 °C under a solar irradiance of $\sim 945 \text{ W m}^{-2}$, along with a daytime net radiative cooling power of up to $\sim 80 \text{ W m}^{-2}$. These results indicate that intrinsic hierarchical porosity in polymeric films provides a scalable and effective structural route for passive radiative cooling applications. Hsu et al.¹⁷⁶ further demonstrated nanoporous PE films with solar reflectance exceeding 0.9,

achieving an outdoor personal cooling of ≈ 2 –3 °C. More recently, Li et al.¹⁵⁰ reported that naturally abundant wood can be processed to form randomized porous structures that result in strong solar backscattering and MIR emissivity leading to 20–60% reductions in building energy consumption. Together, these studies establish intrinsic porosity as a versatile and scalable route for passive RC.

Processing parameters play a decisive role in dictating both the performance and durability of intrinsically porous structures. These parameters refer to the controllable mechanical and thermal conditions applied during polymer deformation—most notably draw ratio, strain rate, and drawing temperature—that govern the processes of void nucleation, growth, and stabilization.¹⁷⁷ Optimized draw ratios (3–10 $\times$, ratio of stretched to initial length) and strain rates (0.1–5 s^{-1}), when applied at drawing temperatures of ~ 0.6 –0.9 T_{m} (relative to the polymer melting point, T_{m}), facilitate stable pore formation while mitigating premature collapse. In semicrystalline polymers such as PE and PP, porosity levels of 60–90% have been reported to reduce the effective refractive index without compromising tensile strength, and crystallinity values of 45–70% provide a balanced compromise between void generation and structural robustness.¹⁷⁸ Importantly, these ranges should be viewed as representative rather than universal benchmarks, as the optimal processing conditions are highly dependent on polymer type, crystalline morphology, and deformation pathway. Postannealing is often employed as a supplementary treatment to stabilize pore geometry and enhance long-term environmental durability.¹⁷⁹ By enabling stress relaxation and partial recrystallization, annealing reduces pore collapse, suppresses defect propagation, and improves resistance to external stresses such as humidity fluctuations and thermal cycling.¹⁸⁰ Typical annealing conditions at 0.4–0.7 T_{m} allow pore walls to consolidate while preserving the hierarchical network essential for broadband solar scattering.¹⁸¹ Effectiveness, however, depends on polymer type and prior history, so annealing is not universally required.¹⁸² Intrinsic approaches remain limited by narrow processing windows and trade-offs between optical efficiency and mechanical integrity.⁷³

3.3.2. Phase Inversion Method. The phase inversion method is a solution-based approach that generates porous architectures through solvent–nonsolvent exchange, in which liquid–liquid demixing induces polymer precipitation and pore formation.¹⁸³ In a typical process, polymers such as poly(vinylidene fluoride-*co*-hexafluoropropylene), poly(ether sulfone), or cellulose acetate are dissolved in a polar solvent (e.g., Dimethylformamide, Dimethylacetamide, or acetone) and deposited by doctor blading, dip-coating, or spraying.¹⁸⁴ Immersion into a nonsolvent bath (commonly water or alcohol) initiates phase separation: rapid solvent–nonsolvent diffusion creates finger-like macrovoids and interconnected channels, whereas slower diffusion produces sponge-like micro/nanoporous networks.¹⁸⁵

Hong et al.¹⁸⁶ demonstrated humidity-tolerant porous polymer coatings fabricated using phase inversion (Figure 5b). The schematic depicts solvent–nonsolvent diffusion that drives polymer-rich and polymer-lean phase separation, and the SEM micrograph shows a heterogeneous porous morphology with interconnected macrovoids and micropores. These hierarchical features provided broadband solar reflectance of 0.93 and the MIR emissivity of 0.96, enabling stable subambient cooling of ≈ 6.5 °C under humid outdoor conditions. Mandal et al.⁷⁸ further developed hierarchically porous cellulose acetate films

that exhibited solar reflectance in excess of 0.92 and cooling powers exceeding 100 W m^{-2} , highlighting their potential for sustainable large-scale deployment. Zhai et al.⁵² introduced a roll-to-roll nonsolvent-induced phase separation process that achieved $\approx 5^\circ\text{C}$ subambient cooling, demonstrating manufacturability at industrial scales. More recently, Hu et al.¹⁸⁷ reported coral-like polyvinylidene fluoride (PVDF) porous films with broadband solar reflectance (~ 0.95), strong MIR emissivity, and antibacterial activity, underscoring the adaptability of this method to multifunctional RC applications.

Optimization requires control of demixing kinetics—solvent out-diffusion and nonsolvent in-diffusion—which shape macrovoids and nanopores.¹⁸⁸ Polymer concentrations of 8–20 wt % balance porosity and stability. Solvent–nonsolvent miscibility determines pore type, bath temperatures ($5\text{--}40^\circ\text{C}$) tune distributions, and polyethylene glycol additives enhance porosity while preventing collapse.¹⁸⁹ Post-treatments such as humidity-controlled drying, mild stretching, and surface functionalization further refine porosity and durability.¹⁹⁰ Despite challenges in solvent recovery and humidity sensitivity, phase inversion offers unmatched scalability, tunability, and compatibility, making it one of the most practical RC fabrication methods.

3.3.3. Template-Assisted Fabrication. Template-assisted fabrication is a bottom-up technique enabling precise nanoscale control over a material's geometric morphology. This control enhances the performance of RC materials, which require the simultaneous optimization of high solar reflectance and selective thermal emissivity.¹⁶⁷ The approach uses two methods: the use of hard templates, forming the final structure's framework, and sacrificial templates, removed after formation.

In hard-template synthesis, the template is fabricated to possess desired properties, acting as the final material's core functional component. AAO is a representative hard template created via an electrochemical process yielding nanoporous alumina membranes.^{165,167,191} The process controls geometry: the interpore distance is determined by the acidic electrolyte, while the pore diameter and film thickness are controlled by the applied voltage and anodization time.^{167,191} A two-step anodization process produces a highly ordered hexagonal pore arrangement, using an initial oxide layer as a pattern for subsequent growth.^{167,191} For RC applications, this method forms a dual-function structure: a transparent infrared emitter (porous alumina) and a solar reflector (the underlying substrate).^{167,191}

Scientific understanding of AAO for RC has progressed. Initial studies by Fu et al.¹⁶⁵ demonstrated porous alumina's cooling potential. Subsequent work focused on performance enhancement. Lee et al.¹⁶⁷ broadened the material's high-emissivity spectrum across the MIR by applying a thin SiO_2 coating via atomic layer deposition. Diaz-Lobo et al. resolved conflicting literature results through chemical control. Their research showed optical properties are tunable, with counterions (e.g., phosphates, sulfates) incorporated from the electrolyte during anodization acting as critical factors. These ions create specific infrared absorption bands that directly shape the material's emissivity profile, establishing design principles for optimizing radiative performance without additional coatings.¹⁹¹

In the sacrificial-template method, porous structures are fabricated by embedding a removable template within a matrix, later eliminated to create a porous network (Figure 5c). This method offers high structural flexibility for tailored pore

structures.^{161,168,192–198} Template material selection involves a trade-off between structural precision, cost, scalability, and process complexity. For low-cost and scalable production, Chen et al. used water-soluble sodium chloride as a template,¹⁹⁹ whereas Yang et al.¹⁹⁴ used sucrose. These materials, mixed with a polymer precursor like PDMS, dissolve in water, leaving a porous structure.

Ordered porous PMMA structures are created by infiltrating a SiO_2 sacrificial template with polymer, followed by hydrofluoric acid etching. Zhang et al.¹⁹² fabricated a periodic inverse opal structure using a 3D colloidal crystal template, achieving 0.94 solar reflectance, significantly outperforming a disordered counterpart (0.77). This showed ordered porous structures provide higher solar reflectance, emphasizing structural control. However, inorganic templates pose challenges like facile removal and precise nanoscale architectural control.¹⁶⁸ To address these limitations, Huang et al. optimized optical properties by forming uniform nanopores in PVDF using metal–organic framework sacrificial templates (Figure 5c). With an optimal pore size of approximately 400 nm and a porosity of 37%, they maximized the solar reflectance from 9.5 to 94.9% and achieved 92.8% thermal emissivity.¹⁶⁸ This demonstrated that precise control over pore size and density is the key to high-performance radiative cooling.^{168,197} In essence, both template approaches confirm a fundamental principle: precise nanoscale architectural control enables high solar reflectance and selective thermal emissivity, providing a robust pathway for RC material design and optimization.

3.3.4. Electrospinning. Electrospinning is a versatile technique using a high-voltage electric field to draw polymer solutions into interconnected microfiber/nanofiber networks. This nanofiber network provides the necessary characteristics for RC. Strong Mie scattering, which results in high solar reflectance, is induced because the fiber diameters are comparable to the wavelengths of sunlight, and this effect is amplified by the network's high porosity and the fiber–air refractive index mismatch^{75,200–209} (Figure 5d). The constituent polymers, such as PVDF and poly(vinyl alcohol), also provide high thermal emissivity in the MIR via molecular vibrations.^{204,206–214} Based on these properties, research has progressed beyond simple cooling films, focusing on improving durability, stability, and integrating multifunctionality.

Electrospinning's material versatility is crucial for robust materials in demanding outdoor/extreme environments. To address polymer fragility/degradation, Xin et al. fabricated durable flexible alumina nanofiber mats (FAFM). As an inorganic material, FAFM resists UV aging and fire while demonstrating strong RC.²¹¹ To withstand extreme space environments, Song et al. developed molecularly engineered polyimide nanofibers with solar reflectance of 99.6% and MIR emissivity of 0.93. This performance is highly durable for space applications. After exposure to severe thermal shock (-196 to 150°C) and corrosive atomic oxygen, the solar reflectance showed minimal degradation (2.2–2.6%) and the material retained $\sim 92\%$ of its mechanical strength.²⁰⁰

Electrospinning facilitates composite/multilayered structure fabrication, ideal for integrating new capabilities. Techniques such as coaxial (core–shell), blended, or roll-to-roll electrospinning are used to develop dynamic and intelligent systems. Zhang et al. developed a textile with high wash stability to improve wearability. After a high-speed (1000 rpm) washing test, the textile's radiative heating performance did not show significant degradation. This study incorporated a Janus

Table 1. Summary of Representative Structural Classes for Radiative Cooling, together with Their Fabrication Routes, Scale-Up Potential, and Representative Use Scenarios

	Multilayer thin film structures	Metasurfaces/nanophotonic structures	Porous structures
Representative fabrication routes	Chemical vapor deposition, ^{47,65} physical vapor deposition, ²²⁹ and others	Photolithography, ²³⁰ Nanoimprint lithography, ¹⁵⁷ Electron beam lithography, ⁴⁹ and others	Electrospinning, ²³¹ phase-inversion, ⁷⁸ and others
Scale-up potential	Limited	Limited to Moderate	High
Representative use scenarios	Buildings, vehicles, and enclose spaces	Photovoltaic integration	Paints/coatings, textiles

structure for stability and selectable heating/cooling.²⁰⁶ Some systems enhance personal comfort by combining radiative cooling with moisture management. Yan et al. used a two-step roll-to-roll electrospinning method to engineer a dual-gradient Janus textile that provides an additional 2.5 °C skin temperature drop through moisture desorption.²⁰² Chen et al. employed microfluidic electrospinning to incorporate hollow microspheres into a double-layer textile, achieving a “self-pumping” effect that promotes evaporation.²¹⁵ For more controllable systems, Pyun et al. demonstrated dynamic radiative cooling with a PDMS nanofiber matrix fabricated via a core–shell electrospinning process. Mechanical pressure reversibly collapses its porous structure, enabling dynamic switching between reflective cooling and transparent noncooling states. The cooling mode achieved subambient cooling of approximately 3.8 °C during the daytime and up to 7.9 °C at night.²⁰¹ In conclusion, electrospinning’s ability to fabricate composite/multilayered nanofiber structures from diverse materials enables direct integration of durability, multifunctionality, and dynamic responsiveness, meeting advanced application demands beyond static cooling.

This review examined four fabrication routes for porous radiative cooling materials, each defined by a fundamental trade-off between optical performance, production scalability, and structural precision. Scalable methods (e.g., phase inversion) offer high throughput but limited microstructural control, whereas template-assisted fabrication provides high precision but is hindered by complexity and cost. Electrospinning serves as a versatile intermediate, offering a platform for the durable and multifunctional systems that are a focus of current research.

Looking forward, material evolution will overcome current design/functionality limitations. Future perspectives include material and structural innovation, such as developing multifunctional composites with integrated properties such as UV resistance, self-cleaning, and flame retardancy.^{216–219} Simultaneously, intelligent/switchable systems will advance, aiming to create adaptive materials for diverse climates, preventing overcooling for year-round efficiency.^{214,220–224}

The practical application of these advanced materials, however, depends on advancements in cost-effective and scalable manufacturing. This requires the adoption of new mass-production technologies such as 3D printing and melt processing. Unlike conventional multistep methods, these approaches enable the continuous and scalable production of digitally designed porous structures, ideal for industrial applications.^{225,226} These manufacturing innovations are expected to expand the role of porous RC materials beyond buildings to diverse fields such as automobiles, electronics, and smart textiles, establishing them as a key technology for an energy-efficient and sustainable future.^{163,203,207,226–228}

To facilitate cross-comparison among the representative RC structural classes discussed above, Table 1 summarizes their representative fabrication routes, scale-up potential, and representative use scenarios. This qualitative overview highlights

the distinct structural characteristics associated with multilayer thin film, metasurface/nanophotonic, and porous RC platforms.

4. FUNCTIONALITIES OF RC

4.1. Spectral Control-Based RC

4.1.1. Selective Mid-Infrared Regulation. Ya Huang, Siming Zhao, and Rufan Zhang

RC emitters were typically classified into three types, i.e., nonselective emitters, monoselective emitters, and dual-selective emitters according to their MIR emissivity (Figure 6a).²³² Nonselective emitters exhibited high emissivity across the entire MIR range, not only enabling large radiative heat loss but also including wavelengths strongly absorbed by atmospheric gases. Monoselective emitters confined high emissivity within the first AW, 8–13 μm while suppressing emission elsewhere, thereby maximizing net cooling under clear-sky conditions. Dual-selective emitters extended this strategy by exhibiting high emissivity in both the first (8–13 μm) and the second (16–25 μm) AWs, with low emissivity outside these windows. Because the radiative effectiveness of each strategy was strongly influenced by atmospheric transparency and humidity, its relative advantages became climate-dependent. Consequently, monoselective designs were effective in moderately humid environments, and dual-selective designs were particularly advantageous in arid or low-humidity climates. The underlying design principles and representative material systems of the mono and dual-selective approaches are discussed in this section.

4.1.1.1. Mono-Selective RC Emitter. Monoselective RC materials exhibit high emission in the first AW regions, while maintaining low emission in nonfirst AW regions.²³³ Specifically, the monoselective materials should have three characteristics in the spectrum: (1) high solar reflectivity to minimize the solar absorption and the resulted heating effects; (2) high emissivity in the first AW regions to enhance the thermal radiation dissipation; (3) low emissivity in nonfirst AW regions to resist the parasitic heat from surroundings. According to their material composition, monoselective RC materials can be divided into two types: polymer-based and inorganic oxide-based materials. In 2014, Fan et al. first reported the monoselective RC materials composed of SiO₂ and HfO₂ via the multilayer photonic structure. They achieved a high emissivity of 0.75 in the first AW regions and a high solar reflectivity of 0.97, thus resulting in the first report of subambient cooling effect under the sunlight.²⁴ Since then, numerous efforts have been devoted to increasing the solar reflectivity and the first AW emissivity, while decreasing the cost of the material preparation.^{17,234} In 2022, Huang et al. developed a solution-processed inorganic emitter to achieve subambient RC, which showed a high solar reflectance (96.4%) and strong infrared-selective emittance (94.6%) with superior spectral selectivity (1.46).²³⁵ The all-inorganic narrowband emitter comprised the SiO_xN_y and a self-assembly monolayer of SiO₂ via

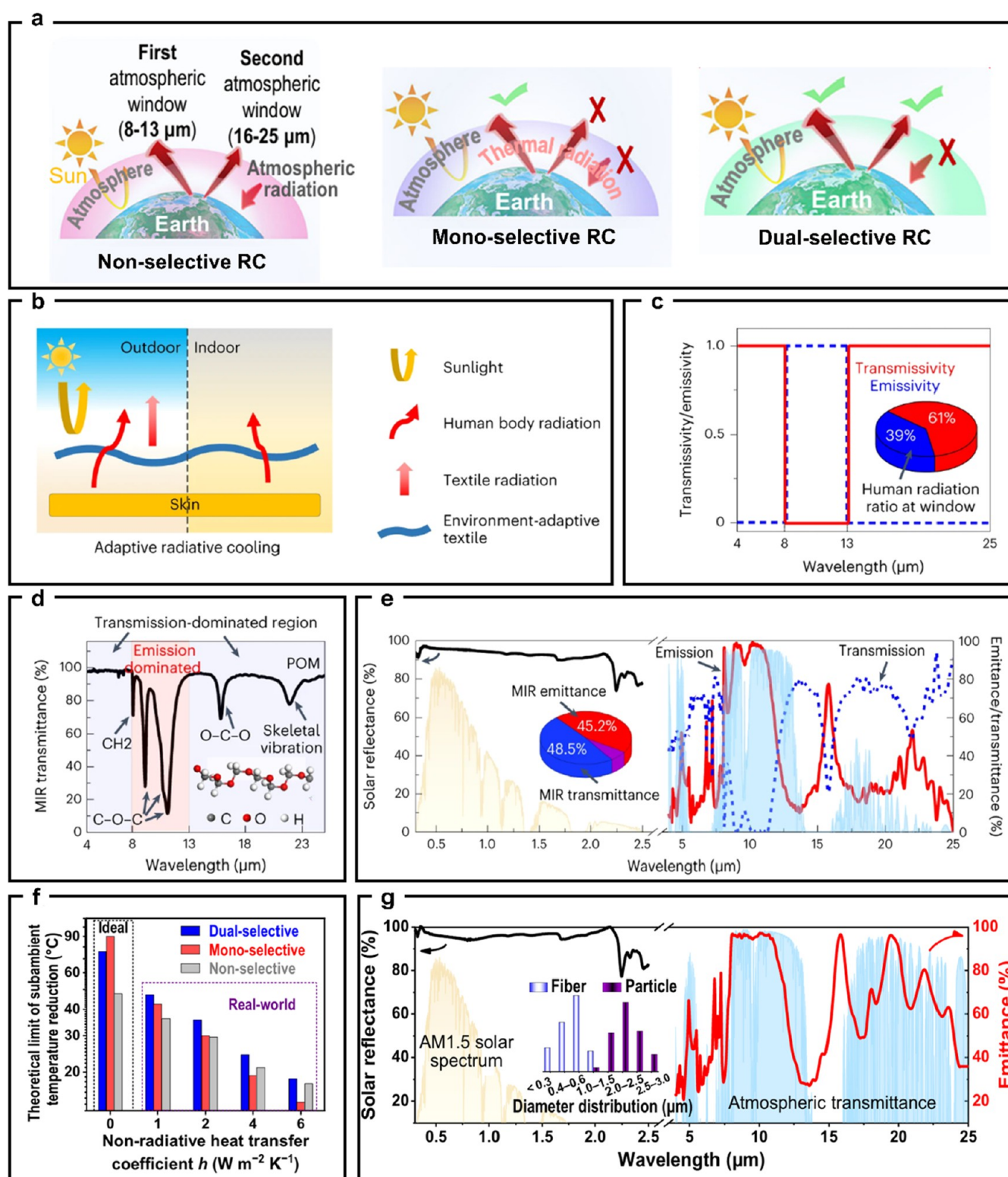


Figure 6. (a) Schematic of the radiative heat transfer process of a nonselective, a monoselective, and a dual-selective radiative emitters. (b) Schematic of the monoselective radiative emitters. (c) Spectral in the MIR band of the monoselective radiative emitters. (d) The FTIR of the POM fabrics. (e) Spectral of the POM film in the 0.3–25 μm . (f) Theoretical calculation of subambient cooling of the three radiative emitters at different heat transfer coefficients ($h = 0-6 \text{ W m}^{-2} \text{ K}^{-1}$). (g) Spectral of the POM-PTFE-Al film in the 0.3–25 μm . (b–e) Reproduced with permission from ref 238. Copyright 2023 Springer Nature. (a) and (f, g) Reproduced with permission from ref 132. Available under CC BY 4.0 license. Copyright 2024 The Author(s).

a simple method rather than the delicate methods. Polymer-based monoselective RC materials were also widely reported for their high processability and scalability. Typically, Zhu et al.

developed the poly(ethylene oxide) (PEO)-based electrospinning nanofibers, which showed great solar reflectivity (96.3%) and the first AW emissivity (78%).²³⁶ Except for the

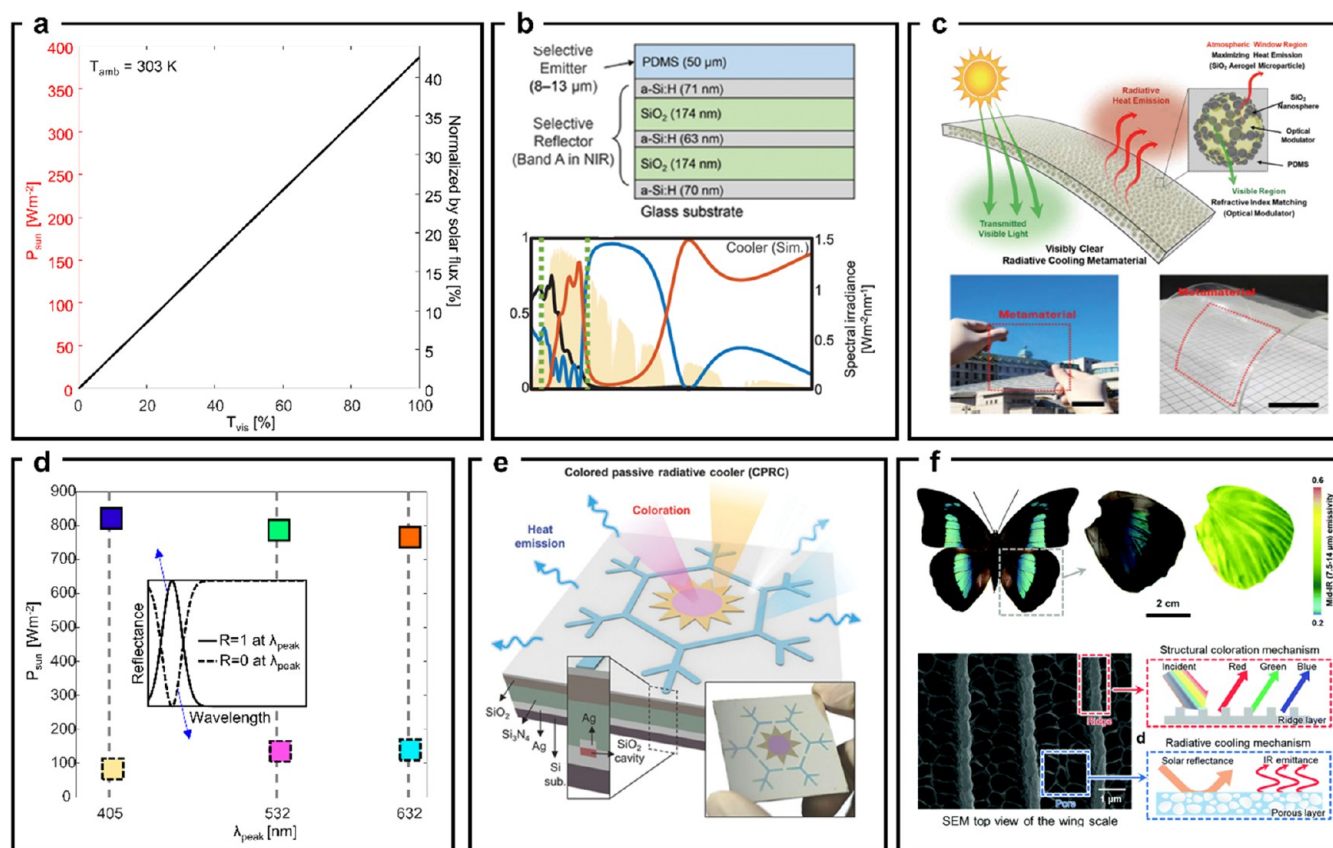


Figure 7. Transparent and colored radiative cooler. (a) P_{sun} for various average visible transmittance with perfect UV and NIR reflection and perfect absorption in the 8–13 μm range. The right axis shows P_{sun} normalized by that of a perfect absorber. (b) A multilayer-based transparent radiative cooler and simulated optical response. Adapted with permission from ref 47. Copyright 2021 John Wiley and Sons. (c) Particle-based transparent radiative cooler and its photographs. Adapted with permission from ref 34. Copyright 2022 John Wiley and Sons. (d) P_{sun} of a colored radiative cooler with various resonant spectra and a bandwidth of 100 nm. The color of markers indicates the reflected color. (e) A multilayer-based radiative cooler with a color printing and its photograph. Adapted with permission from ref 31. Copyright 2018 John Wiley and Sons. (f) A colored radiative cooler inspired by butterfly wing scales. Reproduced with permission from ref 196. Copyright 2022 Royal Society of Chemistry.

material preparation, the property in nonfirst AW regions of the selective monoselective RC materials was also important when applied in practical applications, which attracts much research interest.²³⁷ The low emission in the nonfirst AW region can exhibit high reflection or high transmission, which plays different roles in different scenarios. Taking personal thermal management as an example, our group reported a selective emission model to achieve heat dissipation indoors and outdoors (Figure 6b).²³⁸ It achieved the cooling effects outdoors via heat dissipation in the first AW regions and sunlight reflection, while it achieved temperature reduction indoors via the heat transmission from the human body in nonfirst AW regions (Figure 6c). Due to the backbone chain consisting only of C–O–C bonds, we selected polyformaldehyde (POM) to combine both working modes of emission and transmission (Figure 6c). The POM textile showed a selective emittance (75.7%) in the first AW and a transmittance of 48.5% in the 4–25 μm (Figure 6d), exhibiting enhanced radiative human body cooling performance. Moreover, as the heat-island effects become more and more severe, the surroundings become heating resources for human beings in the city. Hsu et al. developed a selectively emissive and reflective fabric with a high spectral selectivity ratio of 2.23 and an average emissivity of 0.85 in the first AW to achieve the heat dissipation to outer space, while it had high reflectivity outside the first AW to resist the heat transfer.²³⁹

4.1.1.2. Dual-Selective RC Emitter. Although numerous efforts to monoselective RC materials have been made, the cooling contribution of the second AW (16–25 μm) was often neglected in previous studies, as its atmospheric transparency decreased with increasing humidity due to the strong absorption of thermal radiation by water vapor in this spectral range.⁴⁴ However, we demonstrated that under practical conditions (heat transfer coefficient $h \geq 1 \text{ W m}^{-2} \text{ K}$), the dual-selective RC model exhibited markedly superior subambient cooling compared with both nonselective and monoselective RC models.¹³² Specifically, at $h = 1\text{--}6 \text{ W m}^{-2} \text{ K}$, it achieved temperatures 1.0–10.9 °C lower than the nonselective model and 4.2–5.5 °C lower than the monoselective model. Based on this, we developed a scalable polyformaldehyde–polytetrafluoroethylene–aluminum (POM–PTFE–Al) dual-selective thermal emitter. Specifically, POM exhibits strong C–O–C bond vibrations in the first AW, while PTFE shows pronounced C–F bond absorption in the second AW. Both polymers display negligible absorption outside atmospheric windows, enabling the emitter to achieve an emittance of 83.2% in 8–13 μm , 67.5% in 16–25 μm , and a high solar reflectance of 95.4% in 0.3–2.5 μm . It achieved ~ 9 °C daytime subambient cooling and 151.8 W m⁻² net cooling power, outperforming mono- and nonselective designs.

Beyond intrinsic molecular vibrational selectivity, ordered nanophotonic architectures could further enhance RC through

precise spectral control, such as photonic crystals and metamaterials. Mira et al. designed a multilayer cooler composed of three dielectric layers (SiN, SiC, SiO₂) on an Ag back reflector, with thicknesses optimized via a genetic algorithm.²⁴⁰ The device exhibited high emittance in both the first and second AW, delivering strong cooling performance across diverse environments, particularly in arid regions. Its pronounced angle-dependent emittance in the second AW helped suppress ground emission absorption, thereby improving cooling efficiency. Similarly, Yin et al. developed an emitter with triangular prism metamaterials atop a multilayer stack for RC.²⁴¹ The surface features with two triangular prisms acting as an absorption layer on Si₃N₄ and TiO₂ films, while an underlying SiO₂ metamaterial layer extends the absorption band, with its geometry tuning the emission peak. The base slit of the prisms enhances selective emission in the second AW, whereas the Si₃N₄ layer boosts absorption in the first AW. As a result, the emitter achieves absorptances of 98.56 and 96.31% in the 8–13 μm and 16–25 μm bands, respectively, while maintaining solar reflectance above 93%.

As discussed above, numerous studies have been devoted to establishing and developing high-performance selective PC materials, including the monoselective and dual-selective materials. However, an easy, cost, large-scale, stable, and accessible method to obtain the materials is also the biggest obstacle in the way to achieve the practical application of selective PC materials.

4.1.2. Spectral Control-Based RC. Juhoon Baek and Minkyung Kim

4.1.2.1. Transparent RC. While perfect solar reflection is essential for an ideal radiative cooler, it restricts implementation of coolers into applications that require visible transparency, such as windows, displays, and photovoltaic modules. To overcome this limitation, transparent radiative coolers that emit thermal radiation through the atmospheric window while remaining transparent in the visible range have been proposed. Unlike the night-time radiative coolers reported in the 1970s and 1980s,^{11,12,242–244} transparent radiative coolers generally employ spectrally selective control in the solar regime. Thus, while transmitted visible light gives rise to heat gain and reduces the cooling effect, leading to an inevitable trade-off between transparency and cooling (Figure 7a), they can still achieve effective daytime cooling by reflecting the solar spectrum outside the visible.

The early stage of the visibly transparent radiative coolers focused on their integration into solar cells.^{230,245} Since 2020, multiple groups have reignited the interest independently by implementing silica microspheres in a PET film,²⁴⁶ using an ITO layer,²⁴⁷ and employing a Bragg reflector.⁴⁷ These coolers exhibit common optical characteristics across broad wavelength ranges: visible transparency, NIR reflection, and high emissivity within the atmospheric window. Multilayer structures have been widely studied to realize selective NIR reflection. Kim et al. demonstrated that a Bragg reflector, composed of alternating low- and high-refractive-index layers on a PDMS substrate, reduced the temperature by up to 14.4 °C under direct sunlight, compared with bare PDMS (Figure 7b).⁴⁷ Other strategies include the use of optical topological transition in metal–dielectric multilayers, which creates a sharp transition between visible transmission and NIR reflection,^{99,100} or utilizing the intrinsic optical properties of ITO.⁵⁹ The design of multilayers has benefited from various optimization techniques such as quantum computing,^{248,249} genetic algorithms,^{102,250} binary

optimization–based active learning,²⁵¹ particle swarm optimization,⁴⁷ and deep reinforcement learning.¹³⁴ In addition, multilayer-based transparent radiative coolers have been engineered to enhance color neutrality,⁵⁶ introduce diffusive properties,¹³⁶ and provide multifunctionality—for example, switching between radiative conduction and barrier under different thermal conditions⁹⁷ or serving as direction-dependent MIR emitters.²⁸ Multilayer-based coolers often maintain high transmittance in the entire solar spectrum, not limited to the visible, yet they have demonstrated subambient cooling throughout the day.⁶⁵ Beyond multilayers, photonic crystals have also been applied to achieve selective solar reflection.⁹⁸

Fabrication of multilayer and periodic structures typically requires patterning, multiple manufacturing steps, and/or vacuum-based techniques, which makes low-cost scalability challenging. As such, intensive efforts have been devoted to developing transparent radiative coolers using cost-effective approaches such as roll-to-roll processing²⁴⁷ and colloidal self-assembly.²⁵² To induce strong absorption in the atmospheric window while keeping visible transparency, particle- and porous-based structures have been widely investigated. For example, when placed on top of a solar cell, silica aerogel microparticles in a silicone elastomer showcased a temperature reduction of up to 6.2 °C, under direct sunlight, compared with a bare cell (Figure 7c).³⁴ Other approaches include embedding SiO₂ micro/nanoparticles in polymer matrices,^{54,131,253} using delaminated aerogel films,²⁵⁴ and implementing pyramidal patterning.^{255,256} While such particle- or porous-based coolers are not ideal for cooling since they lack spectral selectivity and remain generally transparent in the broad solar spectrum, similar to night-time radiative coolers, they offer practical advantages. Their compatibility with scalable fabrication methods makes real-world deployment more feasible, and their flexible and foldable forms demonstrate potential for applications in displays.¹³¹

4.1.2.2. Colored RC. More sophisticated spectral control within the solar range—for instance, introducing a resonant reflection peak or dip in the visible region—enables coloration of radiative coolers. Vivid coloration, however, requires a narrow reflection peak, which typically accompanies absorption at other wavelengths, leading to a trade-off between coloration and cooling (Figure 7d). Using a reflection dip at a same target wavelength reduces solar absorption and is therefore advantageous for cooling but results in less vivid, subtractive colors. However, the one-to-many relationship between color and spectrum indicates that the vividness of colors does not necessarily lead to a reduced cooling effect, which demonstrates the potential of photonic spectral control for thermal applications.²⁵⁷

Colored radiative coolers can be realized by integrating spectrally selective photonic structures with pigments or dyes,^{78,132,258–260} in which the photonic structures provide cooling via thermal radiation through the atmospheric window and NIR reflection, while preserving the colors from the pigments or dyes. Beyond these pigment-based coolers, various photonic concepts such as multilayer-based spectral selectivity and structural coloration have been demonstrated. To avoid an intensive solar heating, the first proposal of colored radiative coolers used printing, in which only a small portion of the cooler surface exhibits color (Figure 7e).³¹ Tuning a thin-film optical cavity within a multilayer structure enabled the realization of cyan, magenta, and yellow colors and resulted in subambient cooling of 3.9 °C under daylight conditions. More recently, diverse photonic structures including multilayers and periodic

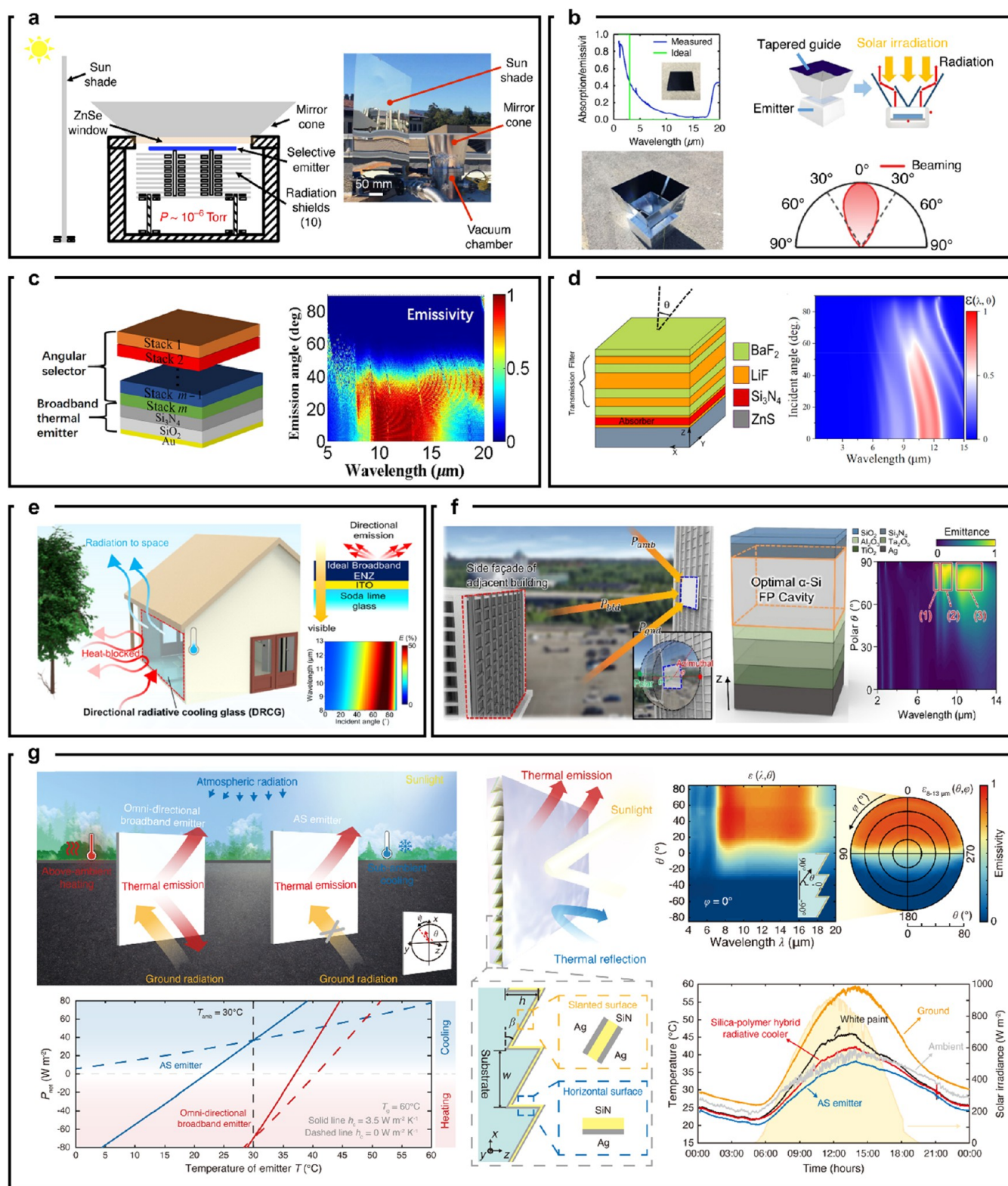


Figure 8. Directional radiative cooling. (a) Schematic of the radiative cooling setup designed to minimize parasitic heat losses, solar irradiance and sky radiation from higher zenith angles. Adapted from ref 44. Available under a CC-BY 4.0 license. Copyright 2016 The Author(s). (b) Schematic of the cooling system with tapered waveguide structure for thermal emission beam control and suppression of solar input. Adapted with permission from ref 276. Copyright 2019 Springer Nature. (c) Left: Schematic of a directional radiative cooler consisting of a broadband thermal emitter at the bottom and a multilayer angular selector on the top. Right: Spectral and angular emissivity of the cooler. Adapted with permission from ref 286. Copyright 2020 American Physical Society. (d) Left: Schematic of a spectrally and angularly selective radiative cooler consisting of a transmission filter on top of a thermal emitter. Right: Spectral and angular emissivity of the cooler. Adapted from ref 287. Available under a CC-BY 4.0 license. Copyright 2022 The Author(s). (e) Schematic of the directional radiative cooling glass for energy-saving windows. Adapted with permission from ref 300. Copyright 2024 De-Gruyter. (f) Schematic of the directional radiative cooler with the oblique radiation-angled photonic structure for building façade. Adapted from ref

Figure 8. continued

301. Available under the Optica Open Access Publishing Agreement. Copyright 2024 Optica Publishing Group. (g) Left: Design considerations for subambient daytime radiative cooling of vertical surfaces. Middle: Schematic of the AS emitter consisting of a sawtooth grating covered by a UV–vis–reflective, IR-transparent nanoPE film. Right: Spectral and angular emissivity distribution and subambient daytime radiative cooling performance of the AS emitter. Adapted with permission from ref 20. Copyright 2024 The American Association for the Advancement of Science.

patterns have been designed for selective absorption of visible light to realize coloration, aided by parametric sweeps,^{261,262} iterative parameter optimization,^{57,263} and AI-based inverse design.^{135,264}

A colored radiative cooler consisting of a monolayer polystyrene microspheres on a PDMS film was demonstrated, where the diameter of the microspheres determined the resulting color.²⁶⁵ The cooler achieved a temperature reduction of 9–27 °C compared with commercial paints of similar colors. In other study, truncated SiO₂ microcones fabricated by a self-assembly method, when coated with an Ag layer, showed subambient cooling under sunlight along with angle-dependent color variation between incidence and observation, after coated by an Ag layer.²⁶⁶ Design strategies have often involved biomimetic approaches inspired by natural structures,²⁶⁷ diffusion using cholesteric liquid crystals,²⁶⁸ the use of phase-change materials,^{269,270} or the photonic bandgap effect.²⁷¹ A hybrid design that combines a PDMS photonic grating with a porous structure inspired by butterfly wing scales was also reported (Figure 7f).¹⁹⁶ Precise pitch control of the grating, combined with the porous structure, produced vivid coloration and solar reflection, which in turn enabled subambient cooling of up to 8.45 °C under sunlight. Very recently, inspired by the scarab beetle, a layered porous nested structure composed of 3D spherical photonic crystal on a PMMA substrate was proposed.²⁷² The structure demonstrated subambient cooling accompanied by angle-dependent color variation. These studies demonstrate that integration of radiative cooling with structural coloration provides a promising pathway to broaden the functionality of radiative coolers and to accelerate their translation into real-world applications.

4.2. Directional RC

Fei Xie, Longnan Li, and Wei Li

Beyond spectral selectivity, the design of directional thermal emission is equally crucial for achieving high-power subambient radiative cooling, particularly in environments where surrounding objects are hotter than the radiative cooler itself. Conventional radiative coolers typically exhibit omnidirectional thermal emission, radiating heat uniformly in all directions. Consequently, they also absorb thermal radiation from all directions according to Kirchhoff's law. This leads to unwanted heat absorption from specific directions, significantly limiting cooling power. For instance, even within the atmospheric transparency window (8–13 μm), the angle dependence of atmospheric transmittance results in significant downward atmospheric radiation at high zenith angles that can exceed the cooler's outgoing radiation.^{4,41} Furthermore, in practical applications like building facades, conventional coolers readily absorb heat from relatively warm ground surfaces and adjacent objects, rendering them ineffective for cooling. Directional thermal emission control can address these limitations by tailoring the spatial distribution of emitter's thermal emission to specific scenarios. Fan et al. highlight the central role of the emissivity profile in controlling the performance of the radiative cooler.⁴

This approach concentrates thermal radiation in the most transparent direction of the atmosphere while minimizing absorption from undesired directions, thereby maximizing net cooling power and unlocking new opportunities for radiative cooling.

Over the past decade, the thermal emission distribution of radiative coolers has been tailored using external devices or by engineering nano/microstructures on emitter surfaces. On the one hand, various types of external devices have been employed to block downward atmospheric radiation originating from high zenith angles.^{35,44,273–278} Chen et al. utilized a mirror-cone to restrict the thermal emission of the emitter to around the zenith direction where the sky is most transparent, thereby preventing relatively high-intensity incoming sky radiation from high zenith angles (Figure 8a).⁴⁴ Zhou et al. integrated a spectrally selective film with a tapered waveguide to achieve the beaming effect on the mid-infrared radiation and the suppression of the solar input (Figure 8b). This system can collimate and confine thermal radiation from the planar emitter within a relatively narrow angular range, thereby reducing the surrounding environment's impact on cooling performance.²⁷⁶ In addition, V-shaped structure has also been demonstrated as an effective means of tailoring the spatial distribution of thermal emission, thereby enhancing radiative cooling performance.^{277–280} On the other hand, thanks to significant advances in thermal radiation control over the past two decades, a range of approaches have been explored to tailor the angular response of thermal emission.^{281–285} This development has enhanced the net cooling power of directional radiative coolers in various application scenarios. For instance, Qu et al. theoretically designed a directional thermal emitter featuring a multilayer angular selector made of anisotropic material placed atop a three-layer broadband thermal emitter (Figure 8c).²⁸⁶ This directional thermal emitter exhibits high emissivity at emission angles between 0 and 40°, enabling it to reflect the strong thermal emission from the surrounding buildings and achieve higher cooling efficiency than conventional radiative coolers with omnidirectional thermal emission. Chamoli et al. designed a 16- μm -thick thin film stack comprising an angle dependent transmission filter overlaid on a selective thermal emitter, achieving both angularly and spectrally selective emission under s- and p-polarized light without the use of anisotropic layers (Figure 8d).²⁸⁷ Fan et al. developed a compact pixelated directional microemitter that exhibits polarization independent thermal emission with strong directionality. Through delicate structure designing, the emitter confines thermal radiation to a narrow angular range across an ultrawide working wavelength range, enabling efficient thermal energy transfer and offering the potential to enhance the capabilities of radiative cooling.²⁸⁸

While radiative cooling has traditionally been applied to horizontal surfaces like rooftops, recent efforts have extended its use to vertical surfaces such as building facades and windows. These vertical applications require more stringent directional control of thermal emission due to their complex heat transfer

processes. The concept of directional thermal emission control based on gradient epsilon-near-zero (ENZ) materials has been explored for use on vertical surfaces. ENZ materials support a leaky p-polarized electromagnetic mode near their resonance pole, known as the Berreman mode, which can couple to propagating free-space modes at a range of wave vectors and certain angles of incidence.^{289–299} Bae et al. designed a directional radiative cooling glass (DRCG) consisting of a multilayer angular selector based on epsilon-near-zero materials (Si_3N_4 and Al_2O_3) deposited on an indium–tin–oxide thermal reflector (Figure 8e).³⁰⁰ The DRCG provides directional emissivity confined to high incident angles while maintaining a visible transmittance above 84%, and its use as a window improves space-cooling performance by approximately 1.5 °C compared with conventional glass. Ryu et al. designed an angular selective broadband emitter by stacking the ENZ layers using a Fabry–Pérot (FP) optical cavity, achieving high emittance at high polar angles (70–90 °) while reflecting radiative heat incident perpendicularly from adjacent buildings (Figure 8f).³⁰¹

Although the approach based on ENZ materials can effectively suppress thermal radiation from adjacent objects, the spatial symmetry and polarization dependence of its thermal radiation pose significant obstacles to achieving subambient radiative cooling on vertical surfaces. To overcome this limitation, several studies^{302–305} have demonstrated relative cooling effects by employing asymmetric directional emitters compared to conventional omnidirectional emitters. To further address the challenge of achieving cooling below ambient temperature, Xie et al. comprehensively analyzed underlying constraints for vertical surfaces and hierarchically designed an angularly asymmetric spectrally selective thermal emitter, demonstrating daytime subambient radiative cooling on vertical surfaces for the first time (Figure 8g).²⁰ These advances underscore the potential of asymmetric directional thermal radiation to enhance radiative cooling performance and highlight its promise for practical building applications.

Overall, the development of directional radiative coolers offers a pivotal solution for overcoming the limitations of traditional horizontal surfaces while unlocking new possibilities for radiative cooling. Current research advances demonstrate that directional thermal radiation is extending radiative cooling applicability to multidimensional scenarios—from rooftops to vertical walls, and from open areas to densely built areas. Moreover, directional thermal radiation shows considerable potential for further development in applications such as vehicles and textiles, where most exterior surfaces are vertical. This enhanced spatial adaptability, combined with optimized spectral selectivity, creates significant opportunities for building energy conservation, electronic thermal management, and sustainable energy systems.

4.3. Adaptive and Switchable RC

Xuzhe Zhao, Jiachen Li, and Kaichen Dong

RC technology utilizes the atmospheric window to exchange heat with the cold outer space, achieving continuous cooling without energy consumption. With the advancement of nanophotonics and the maturation of spectral regulation technologies, RC films have achieved nearly perfect atmospheric emissivity and solar reflectivity, making their cooling power sufficient to meet market demands. With the fast industrialization and real-world applications of RC, new practical requirements emerge and quickly attract wide attention. For example, in high-latitude or midlatitude regions with cold winters, the heat

loss associated with static RC contributes to unwanted heating burden during cold days.³⁰⁶ Consequently, the year-round energy savings of RC are substantially reduced with additional carbon emissions—contrary to the original intention of the RC technology.

To address the above issue, the concept of adaptive and switchable RC (ASRC) was proposed, which involves designing RC devices with tunable atmospheric window emissivity.³⁰ ASRC technologies aim at switching to a thermal insulation mode at low temperatures, and reverting to a RC mode at high temperatures, thereby realizing cooling in summer and keeping warm in winter.

ASRC technologies are generally categorized based on whether external control or actuation is required. Passive ASRC technologies operate autonomously, responding to environmental stimulus such as temperature or humidity without additional energy input. On the other hand, active ASRC technologies require external control—such as mechanical actuation or electrical bias—to modulate thermal emissivity rapidly and precisely.

Among passive ASRC technologies, temperature-adaptive ASRC³⁰⁷ is the most widely adopted due to its direct temperature-emissivity response characteristics, which naturally meets the all-season energy-saving requirements of RC. The working principle of temperature-adaptive ASRC lies in responsive materials or structures whose emissivity varies with temperature. When the ambient temperature falls below a preset threshold, the temperature-adaptive ASRC maintains a low emissivity to minimize thermal loss. Conversely, when the temperature rises beyond the threshold, ASRC autonomously switches to high emissivity to boost RC.

Based on the employed materials or structural mechanisms, temperature-adaptive ASRC can be broadly classified into shape memory material-based technologies³¹⁷ and phase-change material (PCM)-based technologies.³¹⁸ Shape memory materials primarily include shape memory alloys³¹⁹ and shape memory polymers.³¹⁷ For instance, shape memory polymer-based structures integrate a polymer-based mechanical actuation layer between RC and solar heating layers, enabling automatic emissivity switching in response to temperature changes.³²⁰ Zhang et al. developed a dual-mode thermal management device using shape memory polymers that achieved self-switching between heating (859.8 W m^{−2}) and cooling (126.0 W m^{−2}) modes.³²⁰ Shape memory alloys are also commonly used to fabricate mechanical actuators such as memory springs for reversible switching between heating and cooling modes.³¹⁹

PCM-based thermally adaptive ASRC generally employs PCMs like GST,³²¹ perovskites,³²² lanthanum strontium manganese oxide (LSMO),³²³ and vanadium dioxide (VO_2),³²⁴ which have all been extensively explored owing to their drastic infrared refractive index change with temperature changes. With the advancement of nanophotonics and micro-fabrication technologies, a growing number of photonic structures, such as 1D photonic crystals,²⁴ Fabry–Pérot (F–P) cavities,³⁰ core–shell structures,³²⁵ and optical antennas³⁰⁹ have been developed to amplify the emissivity modulation performance of PCMs. Among all the above PCMs, VO_2 , in particular, stands out because of its reversible metal–insulator transition near ambient temperature and pronounced changes in infrared refractive index across its phase transition.³²⁶ In 2018, an F–P cavity photonic structure based on VO_2 was theoretically demonstrated to achieve a modulation depth of 0.6 in emissivity.³⁰ However, early VO_2 -based ASRC designs were

mostly theoretical or small-scale laboratory prototypes, lacking extensive outdoor testing and validation.³²⁷ In 2021, Wang et al.³⁰⁸ and Tang et al.³⁰⁷ independently proposed VO₂-based smart window and roof coatings. As shown in Figure 9a(i),

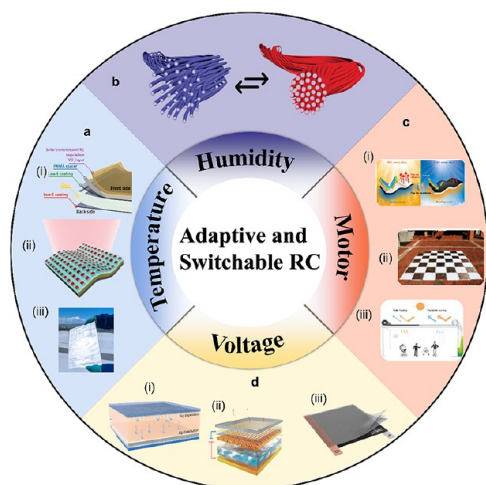


Figure 9. ASRC Technologies with Four Modulation Approaches. (a) Temperature-adaptive ASRC. (i) F–P cavity (ii) metasurface (iii) optical antenna. (b) Humidity-adaptive ASRC. (c) Motor-controlled ASRC. (i) flipping type (ii) sliding type (iii) overlapping type. (d) Voltage-controlled ASRC. (i) reversible deposition of silver (ii) reversible deposition of copper (iii) electro-intercalation. Adapted with permission from ref 307. Copyright 2021 American Association for the Advancement of Science. Adapted with permission from ref 308. Copyright 2021 American Association for the Advancement of Science. Adapted with permission from ref 309. Copyright 2023 Elsevier. Reprinted with permission from ref 310. Copyright 2019 American Association for the Advancement of Science. Adapted with permission from ref 311. Copyright 2022 Springer Nature. Adapted with permission from ref 312. Copyright 2022 American Chemical Society. Adapted with permission from ref 313. Copyright 2020 Springer Nature. Adapted with permission from ref 314. Copyright 2022 John Wiley and Sons. Adapted with permission from ref 315. Copyright 2023 Springer Nature. Adapted with permission from ref 316. Copyright 2021 Springer Nature.

Wang et al.³⁰⁸ proposed a smart window based on a F–P cavity composed of VO₂, PMMA, and a low-emissivity coating, achieving an infrared emissivity modulation depth of 0.4. Tang et al.³⁰⁷ and Li et al.³⁰⁹ realized switchable emissivity with three-layer metasurface and optical antenna structures using VO₂/BaF₂/Ag and PE/VO₂/Al configurations, as shown in Figure 9a(ii) and Figure 9a(iii), respectively, enhancing the emissivity modulation depth to around 0.7. Through year-round energy simulations and outdoor field tests, it was validated that ASRC can reduce overall energy consumption across multiple climate zones worldwide compared with traditional static RC. This is especially effective in regions with large temperature fluctuations, laying the foundation for future ASRC development.

In addition to temperature-adaptive ASRC, humidity-adaptive ASRC offers an alternative passive route for adaptive thermal regulation. Humidity-adaptive ASRC technologies do not respond directly to temperature fluctuations, but instead to the associated changes in ambient humidity.³¹⁰ Given that sweating typically accompanies a rise in human body temperature, humidity-adaptive ASRC materials are often applied in personal thermal management.³¹⁰ Under cool or thermally neutral conditions, limited perspiration keeps humidity-adaptive

ASRC in an “off” state, maintaining low emissivity and conserving body heat. When sweating occurs with a rise in body or ambient temperature, the resulting increase in local humidity activates these materials to an “on” state, raising their emissivity to enhance RC. As illustrated in Figure 9b, Zhang et al. developed a humidity-responsive metafiber by combining carbon nanotubes with hydrophobic triacetate and hydrophilic cellulose, achieving an emissivity modulation depth of 0.35.³¹⁰ Furthermore, Mandal et al. infused porous polymers with volatile liquids such as ethanol or isopropanol, reaching an emissivity modulation depth of 0.64, illustrating strong potential in personal thermal management.³²⁸

Compared with passive ASRC, active ASRC offers distinct advantages in terms of response speed and control precision. Among them, motor-controlled ASRC systems have attracted considerable attention due to their design flexibility and large emissivity modulation depths.³¹¹ These systems typically operate by integrating distinct surfaces with high and low emissivity, switching between them via mechanical structures or manual manipulation. Depending on the switching mechanism, they can be further categorized into flipping-type³¹¹ and sliding-type configurations.³¹²

As illustrated in Figure 9c(i), Xiang et al. developed a Janus all-polymer ASRC material with flipping functionality, utilizing poly(vinylidene fluoride-co-hexafluoropropene) (PVDF-HFP) and polypyrrole (PPy) on opposite surfaces. The chemical bonding differences between the two materials produce spectral contrasts in both the solar and mid-infrared ranges, enabling emissivity modulation via manual flipping.³¹¹ In addition to flipping-based systems, sliding-type structures have also been demonstrated. For example, as shown in Figure 9c(ii), Ke et al. designed a reconfigurable interwoven surface tailored for building thermal regulation, capable of manually sliding to alternate between high and low emissivity.³¹² Li et al. adopted a similar approach as shown in Figure 9c(iii), substituting manual operation with a motorized mechanism to enable emissivity modulation by dynamically overlapping two different roofing materials.³¹³

Similar to motor-controlled ASRC, voltage-controlled ASRC also requires additional energy input to switch between states. Owing to their compact architecture and high response speed, voltage-controlled ASRC has demonstrated broad applicability in aerospace thermal management and smart windows.³¹⁵ Voltage-controlled ASRC can be realized using transition metal oxides,³²⁹ conductive polymers,³³⁰ or reversible metal deposition.³³¹ Among them, transition metal oxides such as WO₃ can significantly increase infrared reflectance upon the intercalation of small cations,³³² thereby enabling emissivity modulation via electrical control. Besides, voltage-controlled ASRC based on conductive polymers offers flexibility and processability that are not achievable with the former. Voltage-controlled ASRC relying on reversible metal electrodeposition typically utilizes infrared-transparent electrodes and aqueous electrolytes.³¹⁴ Without an applied voltage, the device exhibits high emissivity, enabling effective RC at high ambient temperatures; conversely, applying a reverse voltage drives metal layer deposition, lowering the emissivity and thereby promoting heat retention at low ambient temperatures. As illustrated in Figure 9d(i) and Figure 9d(ii), Tao et al.³¹⁴ and Sui et al.³¹⁵ reported emissivity modulation depths of 0.48 and 0.8 using reversible deposition of silver and copper, respectively. Beyond reversible metal electrodeposition, other strategies such as electro-intercalation of lithium ions into graphene layers³¹⁶ as shown in Figure 9d(iii)

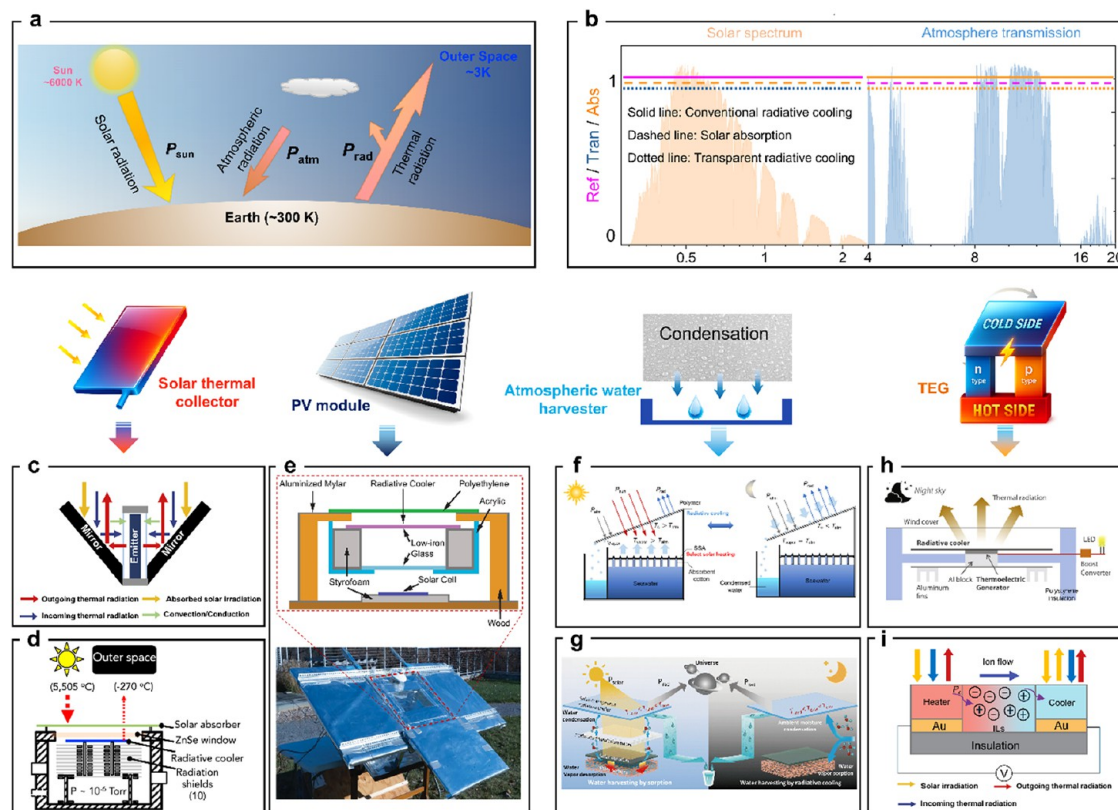


Figure 10. Hybrid and multifunctional radiative cooling (RC) platforms. (a) Schematic illustration of RC coupled with four representative functions on Earth: solar thermal collectors, photovoltaic (PV) modules, atmospheric water collectors, and thermoelectric generators (TEGs). (b) Spectral requirements for conventional radiative cooling, solar absorption and transparent radiative cooling. For solar thermal collectors: (c) vertical RC configurations enabling couitilization of heat and cooling. Reproduced with permission from ref 277. Copyright 2021 Elsevier. (d) Vacuum-assisted RC systems enhancing heat harvesting. Adapted with permission from ref 338. Copyright 2019 Elsevier. For PV modules: (e) transparent RC layers integrated with solar energy conversion. Reproduced with permission from ref 343. Copyright 2024 Elsevier. For atmospheric water collectors: (f) all-day freshwater production via solar-driven interfacial desalination combined with transparent RC. Adapted with permission from ref 339. Copyright 2022 American Chemical Society. (g) Continuous sorption-desorption cycles coupling solar heating with transparent RC. Adapted with permission from ref 341. Copyright 2024 Royal Society of Chemistry. For TEGs: (h) nighttime RC-driven power generation for lighting. Adapted with permission from ref 347. Copyright 2019 Elsevier. (i) Hybrid RC-solar heating architectures for enhanced electrical output. Reproduced from ref 345 under the terms of the CC-BY 4.0 license. Copyright 2023 The Author(s), published by John Wiley and Sons.

and dynamic modulation of intersubband transitions in n-type quantum wells³³³ have also enabled fast and broadband electrical tuning of emissivity.

In conclusion, both passive ASRC (triggered by either temperature or humidity) and active ASRC (operated via mechanical or electrical control) offer distinct advantages tailored to specific applications. Compared with static RC, the dynamic emissivity modulation of ASRC enhances adaptability to varying ambient conditions and facilitates thermal stability. Consequently, ASRC technologies are promising for diverse scenarios, including spacecraft thermal regulation,³³⁴ personal thermal management,³¹⁰ and building energy conservation.³⁰⁷ Nevertheless, their widespread deployment will depend on addressing critical challenges, particularly with respect to durability, scalable manufacturing, and cost-effectiveness. To this end, future research should investigate long-term material stability under realistic operating environments, establish scalable and economically viable fabrication methods, and evaluate integration strategies that enable reliable performance across diverse application scenarios.

4.4. Hybrid and Multifunctional RC

Saichao Dang and Qiaoqiang Gan

Mitigating global warming requires technologies capable of alleviating thermal loads without consuming additional energy.^{32,63,335} RC offers such a pathway by channeling terrestrial heat into outer space through strong mid-infrared (mid-IR) emission within the 8–13 μm atmospheric transparency window, enabling passive—and even subambient—cooling under direct sunlight (Figure 10a). However, the performance of RC is inherently constrained by environmental and spectral conditions. Its cooling power depends strongly on sky clarity, humidity, and ambient temperature, while daytime operation demands stringent solar-band suppression to prevent parasitic heating. As a result, superwhite or spectrally selective coolers must reject most incident solar photons to maintain radiative cooling performance (Figure 10b, solid lines).

In the context of a decarbonizing world, discarding the solar resource represents a profound inefficiency,^{336,337} Furthermore, pure RC systems struggle to meet variable thermal demands across diurnal and seasonal cycles or under fluctuating cloud cover—conditions that limit their practical deployment. These challenges underscore a fundamental reality: no single passive cooling technology can satisfy all thermal management needs across diverse weather and usage scenarios.

The emerging opportunity lies in hybrid and multifunctional RC platforms that preserve the mid-IR radiative channel to the sky while strategically harnessing or redirecting the solar spectrum toward complementary energy services—such as heating,^{277,338} water harvesting,^{339–342} and electricity generation.^{343–349} Recent advances demonstrate that the perceived conflict between radiative cooling and solar utilization is not fundamental, but rather a matter of spectral and thermal management.^{344,350} By spectrally separating the solar and mid-IR bands and minimizing unwanted heat exchange, hybrid RC systems can simultaneously reject excess thermal energy to outer space while capturing useful solar energy for other processes. Building on this framework, the following sections examine four representative directions in RC integration:

- (i) Solar thermal collectors,^{277,338}
- (ii) Photovoltaic (PV) modules,^{343,344}
- (iii) Atmospheric water collectors,^{339–342} and
- (iv) Thermoelectric generators (TEGs).^{345–349}

Each category is discussed in terms of its governing physical principles, material and structural design strategies, and key performance metrics. Together, these examples illustrate how RC can evolve from a single-function passive cooler into a multifunctional thermal–water–energy management platform, offering a more holistic response to the planet's rising thermal and energy challenges.

4.4.1. RC and Solar Thermal Collectors. **4.4.1.1. Physical Principles.** RC requires surfaces with high mid-infrared emissivity and strong solar reflectance (Figure 10b, solid lines), while solar thermal absorbers demand the opposite—strong shortwave absorption and suppressed mid-infrared emission (Figure 10b, dashed lines). This inherent spectral conflict can be resolved by decoupling the solar and mid-infrared channels so that one element captures solar heat while another maintains radiative cooling.³⁴⁴

4.4.1.2. Design Strategies. One strategy is the vertical mirror–emitter configuration (Figure 10c).²⁷⁷ Here, two solar-absorbing wings with high solar absorptivity and mid-infrared reflectivity act as heaters, while a central emitter, designed for high solar reflectivity and strong mid-infrared emissivity, radiates to the sky as a cooler. This geometry separates solar absorption from radiative emission, allowing both processes to operate without interference. Another approach is vacuum-assisted integration (Figure 10d), where a mid-infrared-transparent solar absorber is placed above a radiative cooler inside a vacuum chamber.³³⁸ The vacuum environment minimizes parasitic conduction and convection, preserving large thermal contrasts between the hot and cold elements.

4.4.1.3. Key Performance Metrics. The vertical mirror–emitter system demonstrated enhanced subambient cooling of 6.2 °C (double-sided RC) compared to 4.2 °C (single-sided RC), alongside simultaneous solar heating of ~40 °C above ambient on the absorbers.²⁷⁷ In vacuum-assisted platforms, absorber temperatures reached 24 °C above ambient, while the radiative cooler simultaneously achieved 29 °C below ambient.³³⁸ These results underscore the capability of RC-based architectures to achieve coharvesting of solar heat and sky-coupled cooling within the same footprint.

4.4.2. RC AND PVs. **4.4.2.1. Physical Principles.** RC and PV modules impose opposite spectral requirements: RC relies on reflecting sunlight to remain cool, while PV requires absorbing sunlight for power generation. This competition can be reconciled through transparent RC layers (Figure 10b, dotted

lines), which transmit most of the solar spectrum to the PV cell while maintaining strong mid-infrared emission to the sky.³⁴⁴ In this configuration, the PV continues to harvest sunlight for electricity, while the RC layer simultaneously harvests cold from outer space, enabling colocated solar energy conversion and passive thermal management.

4.4.2.2. Design Strategies. One straightforward strategy employs low-iron glass radiators with high solar transmittance and strong mid-infrared emissivity, laminated above solar cells (Figure 10e).³⁴³ In this configuration, the glass not only transmits sunlight to the PV absorber but also establishes a subambient cavity between the cover and the cell, effectively storing “harvested cold” that can be used to dissipate excess heat from the module. An alternative strategy is to apply transparent RC coatings directly onto the PV cover surface.^{14,230,280,351–353} These coatings—ranging from silica–polymer composites^{34,352} and porous dielectrics²³⁰ to multilayer thin films³⁵¹ and engineered micro/nanostructured textures³⁵³ are designed to enhance the infrared emissivity of the solar cell surface while maintaining high solar transmittance (>90%). By enabling the cell itself to radiatively shed heat to the sky, this approach lowers operating temperature, mitigates thermal degradation, and improves long-term performance.

4.4.2.3. Key Performance Metrics. Outdoor experiments on laminated RC–PV modules demonstrate subambient temperature reductions of approximately 5 °C, with radiative cooling power densities of 60–90 W m^{−2} under peak solar irradiance.³⁴³ Importantly, these systems maintain PV electrical outputs exceeding 150 W m^{−2}, evidencing that effective thermal management does not compromise photovoltaic conversion. The corresponding radiative cooling flux has been measured at 63.8 W m^{−2} under full sunlight and 87.0 W m^{−2} at night, confirming robust 24-h radiative performance. Such thermal regulation translates into efficiency improvements of up to ~30%, along with mitigated thermal degradation and extended module lifetime. Collectively, these findings establish transparent RC coatings and laminates as practical, scalable, and durable solutions for passive thermal regulation in solar energy systems, simultaneously enhancing performance, stability, and sustainability.

4.4.3. RC and Atmospheric Water Collectors.

4.4.3.1. Physical Principles. In atmospheric water harvesting (AWH), the introduction of transparent radiative coolers plays a crucial role in reconciling condensation with daytime solar heating.^{339–342} Transparent RC layers are engineered to be highly emissive in the mid-infrared, ensuring continuous radiative cooling to the sky, while at the same time transmitting most of the solar spectrum to underlying absorbers or sorbent beds.³⁵⁴ This dual function establishes a spectral separation of roles: the solar channel is directed downward to drive evaporation or desorption, while the mid-infrared channel remains open upward to sustain subambient cooling and condensation. In this way, transparent RC components act simultaneously as optical windows and radiative condensers, creating the thermodynamic conditions needed for all-day water harvesting.

4.4.3.2. Design Strategies. In practice, transparent radiative coolers made from polymers such as PDMS and PMMA have been widely employed as the top condenser layer in hybrid water-harvesting modules.^{339,340,355} A representative approach is the all-in-one configuration, where the transparent RC cover both maintains radiative cooling and allows solar radiation to reach an underlying absorber or sorbent bed within an insulated

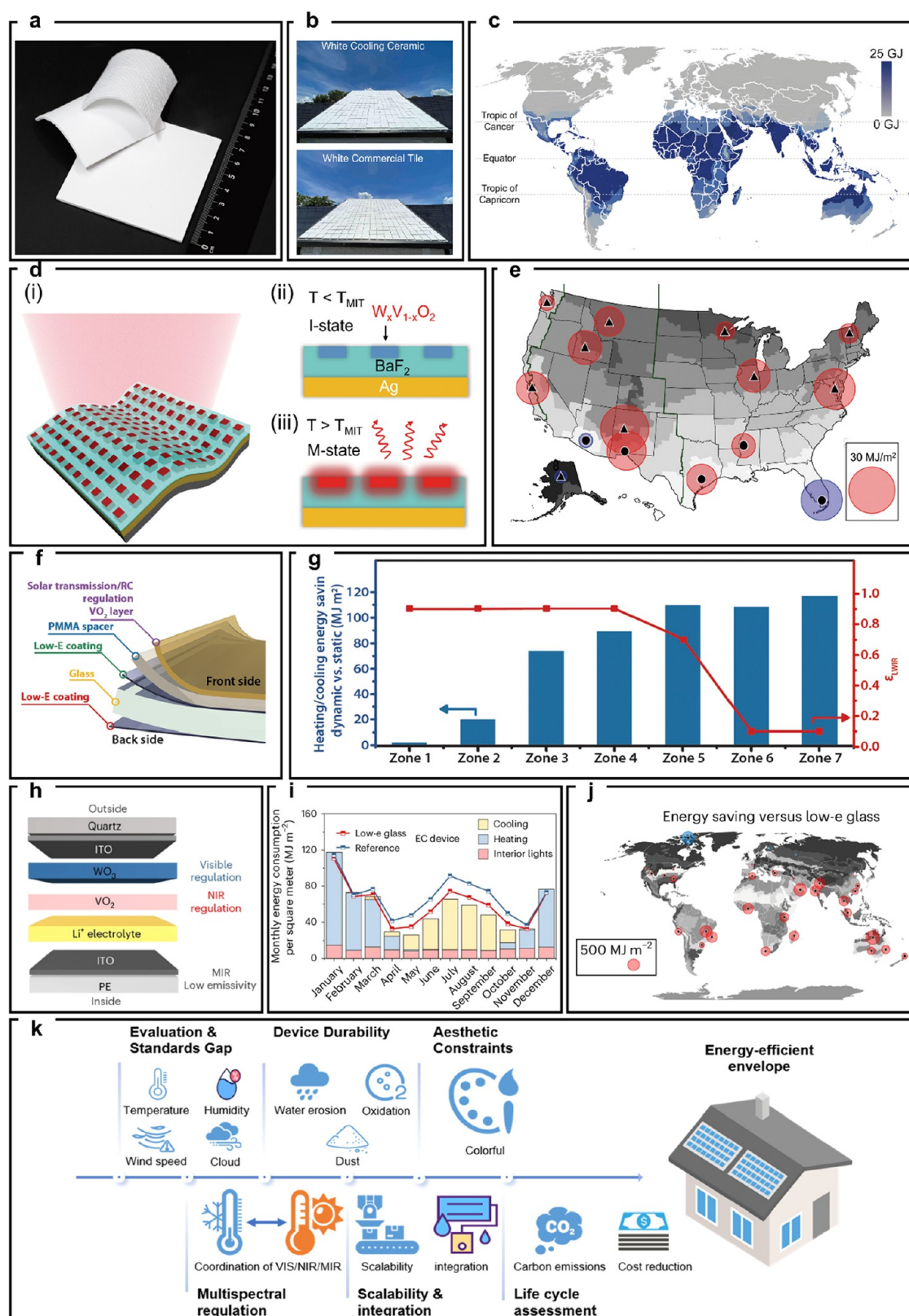


Figure 11. Energy-efficient buildings and smart windows. (a) Photograph of the cooling ceramics with flat and curved shapes. Patterns can also be applied on the cooling ceramic surface. (b) Photograph of the model houses, with the white cooling ceramic and white commercial tile applied on the roof (area: $\sim 1.15 \text{ m}^2$). The model houses were installed 2 m apart during the experiment to eliminate interference. (c) Energy-saving performance on a worldwide scale considering the energy consumed by cooling systems, fans, and heating equipment. Adapted with permission from ref 164. Copyright 2023 AAAS. (d) Schematics of the structure (i), materials composition and working mechanism (ii and iii) of the Temperature-adaptive radiative coating. (e) Minimum space-conditioning source energy savings (SCSES_{min}) of TARC compared with other existing roof-coating materials for different cities representing the 15 climate zones in the United States. Red and blue circles indicate positive and negative SCSES_{min} values, respectively. The values are scaled to the area of the circles. Adapted with permission from ref 307. Copyright 2021 AAAS. (f) Schematic structure of the RC

Figure 11. continued

regulating thermochromic window. (g) Heating and cooling energy saving (blue columns) of simulated optimized dynamic samples against optimized static samples (red square) from zones 1 to 7. In this simulation, T_{sol} was fixed to 30%. The optimized static ϵ sample is derived from the point of minimum total energy consumption by adding heating and cooling in seven climate zones by fixing ϵ . The optimized dynamic ϵ window has a ϵ_{LWIR} of 0.9 for cooling and 0.1 for heating. The optimized dynamic ϵ window has lower energy consumption than optimized static ϵ window from zones 2 to 7. Adapted with permission from ref 308. Copyright 2021 AAAS. (h) Schematics of the optimizing-multispectral EC device with a low-e surface. (i) Monthly energy consumption of the EC device, low-e glass and normal glass window in the climate condition of Shanghai. To provide a clearer representation of the data for this EC device (j) Estimated heating and cooling energy saving of a triband-optimized EC device against a commercial low-e glass as the baseline for different cities representing different climate zones. Adapted with permission from ref 377. Copyright 2024 Springer Nature. (k) Current limitations and future potential of RC for energy-efficient envelopes.

chamber (Figure 10f).^{339,340} This enables daytime vapor generation beneath the cover and condensation on its subambient surface, while at night the same RC layer directly condenses atmospheric moisture. An alternative route is the sorption–desorption cycle, in which hygroscopic materials (e.g., salt–polymer composites,³⁴¹ hydrogels^{356–358}) are combined with transparent RC condensers (Figure 10g). Here, the RC layer provides continuous cooling to enhance nighttime vapor uptake, while solar heating during the day regenerates the sorbent and directs the released vapor to the RC surface for condensation. Key considerations across these designs include the optical transparency and mid-infrared emissivity of the RC layer, the durability of polymeric materials under outdoor conditions, and the optimization of surface wettability and vapor transport channels to maximize condensation efficiency and water yield.

4.4.3.3. Key Performance Metrics. Hybrid RC–AWH systems have demonstrated daily water yields of 0.2–3.6 L m^{−2} day^{−1}, with instantaneous condensation fluxes up to 0.36 L m^{−2} h^{−1} under favorable humidity conditions.^{339–341,356–358} Transparent RC layers, typically composed of polymers such as PDMS or PMMA, serve both as condensers and spectral separators, enhancing subambient cooling and extending dew-point margins by several degrees compared with conventional passive designs.^{339,340,355} Performance assessment typically involves dew-point margin ($\Delta T_{\text{surface}} - T_{\text{dew}}$), net cooling power, areal yield (L m^{−2} day^{−1}), and sorbent productivity (kg H₂O per kg sorbent per cycle). Multiday cyclic experiments confirm stable water output and minimal degradation, underscoring the long-term feasibility and operational robustness of RC-assisted atmospheric water harvesting. Collectively, these findings establish RC as a sky-coupled thermal component that enables sustainable, diurnal freshwater generation across a wide range of climatic conditions.^{35,358,359}

4.4.4. RC and Thermoelectric Generators (TEGs).

4.4.4.1. Physical Principles. TEGs convert a temperature gradient into electricity by driving charge carriers across n–p legs, and their output scales directly with the magnitude and stability of the temperature difference (ΔT).^{347,348} RC provides a natural cold sink: surfaces with high mid-infrared emissivity can emit thermal radiation through the 8–13 μm atmospheric window, allowing them to cool below ambient temperature, particularly under clear skies. However, the ΔT achievable with RC alone is typically modest (~ 1 – 5 °C relative to ambient air), which limits the electrical output of a TEG if RC is used in isolation.³⁴⁸ Hybrid RC–TEG systems overcome this limitation by pairing the RC surface as the cold side with a dedicated hot side, such as a solar-heated absorber^{345,360,361} or the hot ground.³⁶² This configuration maintains a continuous temperature bias: at night, the RC surface cools below ambient, while the hot side—often the surrounding air or residual thermal

mass—remains warmer; during the day, solar heating further elevates the hot side temperature. In this way, RC provides a persistent cold reservoir that sustains ΔT , enabling round-the-clock thermoelectric power generation.^{345,347,349,360,361}

4.4.4.2. Design Strategies. Nighttime configurations typically use a sky-facing RC radiator as the cold side and ambient air as the hot side (Figure 10h).³⁴⁷ Design improvements include enlarging the radiator-to-TEG area ratio, applying IR-transparent covers to suppress convective exchange, and reducing thermal/electrical contact resistances. For daytime operation, spectral separation is critical: solar photons are routed to a selective absorber or thermal mass (hot side), while the RC element remains optically coupled to the sky (cold side).^{345,360,361} Recent advances employ dual-material designs such as cellulose-based composites with opposite optical properties: a solar-reflective, high-emissivity radiator as the cold surface, paired with a solar-absorbing, MIR-suppressing heater as the hot surface (Figure 10i).³⁴⁵ This arrangement maintains a stable ΔT over day–night cycles.

4.4.4.3. Key Performance Metrics. Prototype RC–TEG systems have demonstrated $\Delta T \approx 2$ – 5 °C, producing open-circuit voltages of 80–100 mV and power outputs around tens of mW m^{−2}, sufficient to drive small electronics or LEDs.³⁴⁷ Cellulose-based day–night systems reported a ΔT of ~ 10 °C under solar irradiance of ~ 400 W m^{−2}, generating thermovoltages above 60 mV. Modeling further indicates that with optimized convective management, minimized parasitic losses, and proper thermal impedance matching, outputs could exceed 0.5 W m^{−2} in hot, arid climates.³⁴⁵ Although far below photovoltaics in power density, RC–TEG hybrids uniquely provide continuous 24-h trickle power for sensors, off-grid electronics, and distributed Internet of Things (IoT) devices without external energy input.

5. POTENTIAL APPLICATIONS OF RC

5.1. Energy-Efficient Buildings and Smart Windows

Shaowen Cao and Yi Long

Buildings account for $\sim 30\%$ of global final energy use, and spectral thermal management of envelopes and glazing is increasingly regarded as a priority pathway to reduce carbon emissions.^{8,363} RC provides a continuous and stable passive “cold source” for buildings. For opaque envelopes, RC applied to roofs and walls has demonstrated appreciable temperature reductions and energy savings under real conditions in low-latitude regions.³⁶⁴ In midlatitude climates with distinct seasons, dynamical envelopes that integrate RC and radiative heating are emerging, enabling reversible switching between “cooling” and “heating” states to optimize annual energy performance.³⁶⁵ For transparent systems, thermal-management materials used in smart windows must preserve visible transmittance and daylighting, which demands more complex and precise spectral

control across the VIS, NIR, and MIR bands. In cooling-dominated low-latitude regions, static RC windows are suitable, whereas in midlatitude regions dynamically tunable smart windows are needed to accommodate seasonal variation. It is worth mentioning the recent radiative warming for high latitude regions have been developed with the broadband mode,^{366,367} which is not covered in this review. Consequently, this section reviews RC applications and energy benefits in roofs/walls and smart windows for energy-efficient buildings and examines the system-level potential and engineering challenges for real-world deployment.

For opaque static building envelopes, i.e., RC roofs and walls, the outer layer typically employs coatings, films, ceramic panels, or cementitious components with high solar reflectance (R_{sol}) and high MIR emittance (ϵ_{MIR}), integrated with existing insulation and waterproofing to lower surface temperature and cooling loads without altering building functions. Because roofs and walls are continuously exposed to UV radiation, precipitation, and soiling, long-term durability is critical for real-world deployment. Addressing this need, Tso et al. fabricated hierarchically porous Al_2O_3 cooling ceramics via phase inversion and sintering (Figure 11a,b). The ceramic exhibits weatherability, mechanical stability, and long-term performance. For a four-story apartment prototype in tropical cooling-dominated climates, simulations indicate >10% annual heating, ventilating, and air conditioning (HVAC) energy savings, equivalent to $\sim 25 \text{ GJ yr}^{-1}$ (Figure 11c).¹⁶⁴ Hu et al. reported a solution-processed dual-particle inorganic porous architecture that combines durability with applicator-friendly processing and delivers near-optimal high R_{sol} /high ϵ_{MIR} . In humid climates it achieves $\sim 3.5^\circ\text{C}$ subambient cooling and $\sim 8\text{--}10\%$ reductions in building cooling-related emissions.³⁶⁸ Recently, Li et al. developed a water-borne cementitious integrated cooling paint by embedding nano- BaSO_4 into a porous C-S-H network. The paint reaches $\sim 93\%$ R_{sol} and $\sim 95\%$ atmospheric-window emittance under routine brush application and maintains high mechanical and weathering robustness. Field tests in Singapore show 30–40% reductions in air-conditioning electricity use relative to a commercial cool-roof paint.³⁶⁹

Static RC is effective in cooling-dominated low-latitude regions, yet it can cause winter overcooling penalty in midlatitude climates with distinct seasons and in heating-dominated high-latitude regions.³² This risk increases heating demand and motivates the use of tunable thermal management. VO_2 is a prototypical thermochromic material whose metal–insulator transition enables temperature-dependent emissivity. Leveraging this property, Wu et al. designed a temperature-adaptive radiative coating (TARC) that reversibly switches near 22°C from low emissivity ($\epsilon_{\text{LWIR}} \approx 0.2$) to high emissivity ($\epsilon_{\text{LWIR}} \approx 0.9$)³⁰⁷ (Figure 11d). Annual whole-building simulations across 15 U.S. zones show energy savings of about $22.4 \text{ MJ}\cdot\text{m}^{-2}\cdot\text{yr}^{-1}$ for a typical single-family house in mixed climates such as Baltimore when compared with a static RC coating (Figure 11e). Extending this concept, Wu et al. developed a roll-to-roll flexible overlayer with tunable ϵ_{LWIR} and optimized solar absorption for energy-efficient building envelopes.³⁰⁹ Compared with a standard cool roof it yields additional annual energy reductions in most climate zones, for example $\sim 12.6 \text{ GJ}$ per year for a typical San Francisco residence, while mitigating winter overcooling and cool-roof condensation. In addition, Long et al. proposed a switchable interwoven surface for dynamic cooling–heating regulation.³¹² The surface

is assembled from modules with distinct R_{sol} and ϵ_{LWIR} pairs: Phase 0 exhibits a black, high absorptance state with $A_{\text{sol}} = 0.87$ and $\epsilon_{\text{LWIR}} = 0.39$, whereas Phase 1 exhibits a white, low-absorptance high-emittance state with $A_{\text{sol}} = 0.05$ and $\epsilon_{\text{LWIR}} = 0.91$. Spatial reconfiguration between the two module types enables meter-scale deployment and achieves up to 9.5% annual HVAC energy savings in ASHRAE Climate Zone 4 relative to a conventional roof.

Compared with opaque materials for roofs and walls, thermal management for transparent glazing must preserve daylighting while coordinating spectral control across the VIS, NIR, and MIR bands. From practical considerations, simultaneously achieving high visible transmittance, environment-dependent near-infrared dynamic modulation, and tailored mid-infrared emissivity is challenging. If relatively independent spectral regulation is desired in the VIS, NIR, and MIR bands, at least three optical design degrees of freedom are generally required. In reported transparent glazing structures, common implementations often involve about 4 to 7 design degrees of freedom. This range is not a fixed standard, and it is closely related to the adopted spectral regulation mechanism. If a single functional layer can contribute to multiband regulation, the required degrees of freedom may be reduced accordingly. In contrast, when additional electrochemical circuit elements are introduced to enable multiple states or larger modulation amplitude, the required design freedom typically increases.

Rho et al. reported a static RC window that employs an emitter–reflector stack comprising a PDMS emissive top layer to enhance ϵ_{LWIR} , a $\text{TiO}_2/\text{MgF}_2$ Bragg reflector engineered to maintain high T_{VIS} and selectively reflect NIR radiation, and an apertured Ag reflector to suppress A_{sol} without compromising a neutral appearance or T_{VIS} .⁵⁶ Outdoor measurements showed a 22.1°C temperature reduction relative to a PDMS-coated glass reference. Zhou et al.³⁷⁰ proposed a transparent delignified-bamboo/epoxy glazing that integrates a PMMA-protected AgNW low-emissivity face ($\epsilon_{\text{LWIR}} = 0.3$) opposite a high-emissivity epoxy face ($\epsilon_{\text{LWIR}} = 0.95$) delivering high transmittance ($T_{\text{lum}} = 80\%$) and, in Singapore building-energy simulations, up to $\sim 89\%$ annual energy savings relative to commercial low-e glass. Richards et al. demonstrated a transparent, self-cleaning polymeric photonic metamaterial based on PDMS micropylamids with $T_{\text{VIS}} \sim 95\%$ and ~ 0.98 emissivity in $8\text{--}13 \mu\text{m}$, yielding a theoretical cooling power of $\sim 97 \text{ W}\cdot\text{m}^{-2}$ and $\sim 6^\circ\text{C}$ subambient cooling under humid outdoor conditions in Karlsruhe, highlighting practical potential for passive building cooling and energy reduction.¹³⁶

Compared with static RC windows that provide cooling only, dynamically tunable smart windows are more effective for improving whole-building annual efficiency because they enable high-performance thermal management across diverse climates and weather conditions. Long et al. reported a VO_2 -based smart window³⁰⁸ (Figure 11f). The device comprises a VO_2 thin film, a transparent PMMA spacer, and a glass substrate coated with ITO on both sides, forming a Fabry–Perot cavity. VO_2 serves as the NIR modulation layer, while PMMA and ITO act as MIR-transparent and MIR-opaque layers. Leveraging the VO_2 phase transition and F–P resonance, the window dynamically tunes the T_{sol} and ϵ_{LWIR} with $\Delta T_{\text{sol}} = 9.3\%$ and $\Delta \epsilon_{\text{LWIR}} = 0.4$. Relative to a “static-optimal-emissivity” window, it yields up to $115.9 \text{ MJ}\cdot\text{m}^{-2}\cdot\text{yr}^{-1}$ savings in heating and cooling source energy over a full year. Using commercial low-e glass as the baseline, whole-building simulations report up to $324.6 \text{ MJ}\cdot\text{m}^{-2}\cdot\text{yr}^{-1}$ annual energy savings and superior performance across climate zones

(Figure 11g). In a related thermochromic advance, Long et al. also demonstrated a smart window composed of glass/ITO low-e layers and an hydroxypropyl cellulose (HPC) hydrogel encapsulated in polyethylene.³⁷¹ Outdoor tests show a ~ 5.4 °C reduction in summer relative to clear glass. Building-energy modeling indicates $\sim 37.4\%$ annual HVAC reduction in Singapore, $\sim 18.8\%$ reduction during the heating season in Beijing, and ~ 9.2 – 19.1% total annual energy savings for large office buildings across multiple cities. Despite the promising thermal regulation performance, hydrogel-based smart windows face nontrivial outdoor durability challenges, which directly affect long-term optical stability and practical scalability. Hydrogel-based smart windows face four dominant outdoor durability risks. Dehydration and moisture migration can cause shrinkage and state drift, and commonly reported approaches include device-level encapsulation and edge sealing, as well as hygroscopic modification through hygroscopic functional groups or salt systems.^{372,373} UV and oxidative aging may induce chain scission, yellowing, and network embrittlement, and mitigation approaches include incorporating UV-shielding nanoparticles to enhance UV absorption or scattering.³⁷⁴ Thermal cycling fatigue can trigger microcracks and reduce state stability, and common strategies include network reinforcement and device-level encapsulation.³⁷⁵ Freeze–thaw and overheating can cause irreversible degradation, and organo-hydrogel designs using low-volatility solvents such as glycerol have been reported to improve freezing and drying tolerance.³⁷⁶ These approaches are typically accompanied by constraints including interfacial reflection and sealing reliability, salt crystallization or ion migration, increased process complexity, and viscosity or processability changes.

Apart from thermochromics, Cao et al. introduced a triband electrochromic smart window consisting of quartz/ITO/ WO_3 / VO_2 /solid electrolyte/ITO/PE (Figure 11h).³⁷⁷ The device enables independent control of visible and NIR transmittance and establishes ϵ_{LWIR} outside and low ϵ_{LWIR} inside. Simulations show up to ~ 596.7 MJ·m^{−2} annual heating plus cooling savings versus commercial low-e glass across many climate zones, and for Shanghai the HVAC energy use is reduced by $\sim 23.9\%$ compared with clear glass (Figure 11i,j).

From the perspectives of system integration and commercialization, static RC roofs and walls have already matured into replicable product lines and engineering pathways in cooling-dominated climates, reflecting comparatively high readiness.^{378,379} Static RC glazing has undergone outdoor trials and whole-building energy simulations at multiple sites, yet large-scale market adoption has not emerged. Dynamically tunable roofs/walls and smart windows exhibit year-round energy savings in laboratory but overall remain in an engineering scale-up phase. The key bottlenecks fall into two areas (Figure 11k). 1. Deployment and industrialization constraints persist: long payback periods, poor weatherability, antisoiling and robust cycling³⁸⁰ require rigorous qualification; achieving low-cost, large-area manufacturing with high uniformity and yield remains challenging; compatibility with existing roofing, wall, as well as city-scale aesthetic requirements, limits its applications. 2. Evaluation and standards are insufficient: the translation from material-level temperature reduction to building-level energy savings is not well-defined as the performance is highly sensitive to convection, humidity and cloudy weather, as well as mounting details and sensor placement.

Collectively, these considerations suggest a pragmatic development pathway. In cooling-dominated regions, prioritize

scaling static RC roofs and walls while completing weathering, fire certifications, and life-cycle carbon footprint assessment. In midlatitude regions with pronounced seasonality, dynamically tunable building envelopes and smart windows should be developed with large modulation in both solar (0.25 – 2.5 μm) and MIR (2.5 – 25 μm) bands. In parallel, shift evaluation from short-term temperature modulation to hourly loads and annual whole-building energy simulation under transient outdoor conditions. On the technological side, cost-effective and environmentally friendly materials together with scalable and compatible process are the keys to lab to fab transfer.

Assessing deployment readiness for radiative cooling building envelopes and smart windows hinges on manufacturability, durability, and climate-specific constraints. Static opaque RC envelopes are relatively scalable because they can use low-cost solution processing such as brush coating.^{368,369} By contrast, dynamically tunable smart windows are limited by expensive active materials such as VO_2 and WO_3 , and by complex multilayer deposition and integration.^{308,377} In real environments, performance is challenged by UV exposure and soiling, and hydrogel-based systems additionally face dehydration and freezing, with reported mitigation routes including robust cementitious binders, hygroscopic salt doping, and UV-shielding nanoparticles.^{164,369,372,373,375,376,381} A key barrier for opaque envelopes is winter overcooling in midlatitudes, motivating temperature-adaptive radiative coatings.^{307,312} For glazing, maintaining daylighting while enabling NIR modulation and tailored MIR behavior often requires multilayer asymmetric stacks of roughly four to seven functional layers.^{56,377} Overall maturity differs markedly: static opaque roofs are closest to deployment, static RC glazing is moving through field testing, and dynamically tunable smart windows remain in engineering scale-up.

5.2. Vehicles and Enclosed Spaces

Hyunkyung Kwak, Do Hyeon Kim, and Young Min Song

Thermal regulation technologies in enclosures are essential for ensuring thermal comfort of human lives and durability of electronic devices. The ideal temperature range where humans experience thermal comfort is typically known as 22 – 26 °C.³⁸² In addition, various electronic devices (e.g., smartphones, laptops, and electric vehicles) can effectively operate from 20 to 40 °C due to the ideal operating temperature range for Li-ion batteries.³⁸³ However, during summer, the enclosure temperature can rise extremely higher than that range without any cooling source. For instance, the indoor temperature of a vehicle parked under direct sunlight can even reach ~ 90 °C in summer,³⁸⁴ causing a risk of heat-related illnesses and $\sim$ degradation of device performance.³⁸⁵ Moreover in winter, the indoor temperature of buildings can drop to near 0 °C or even lower,³⁸⁶ inducing hypertension-related and respiratory disease, depression, and anxiety.³⁸⁷ In general, HVAC systems can provide thermal comfort in enclosures but require a significant amount of energy for operation. According to the previous report, the energy used for thermal regulation accounts for $\sim 20\%$ of building energy consumption, and if this trend continues, it is predicted to increase to 50% by 2050.³⁸⁸ Such energy demands lead to serious environmental problems such as greenhouse gas emissions and an acceleration of global warming. To realize energy-efficient thermal regulation in enclosures, passive radiative cooling/heating has been explored in various ways. A common method for passive radiative cooling to mitigate the overheating issues is applying radiative coolers to

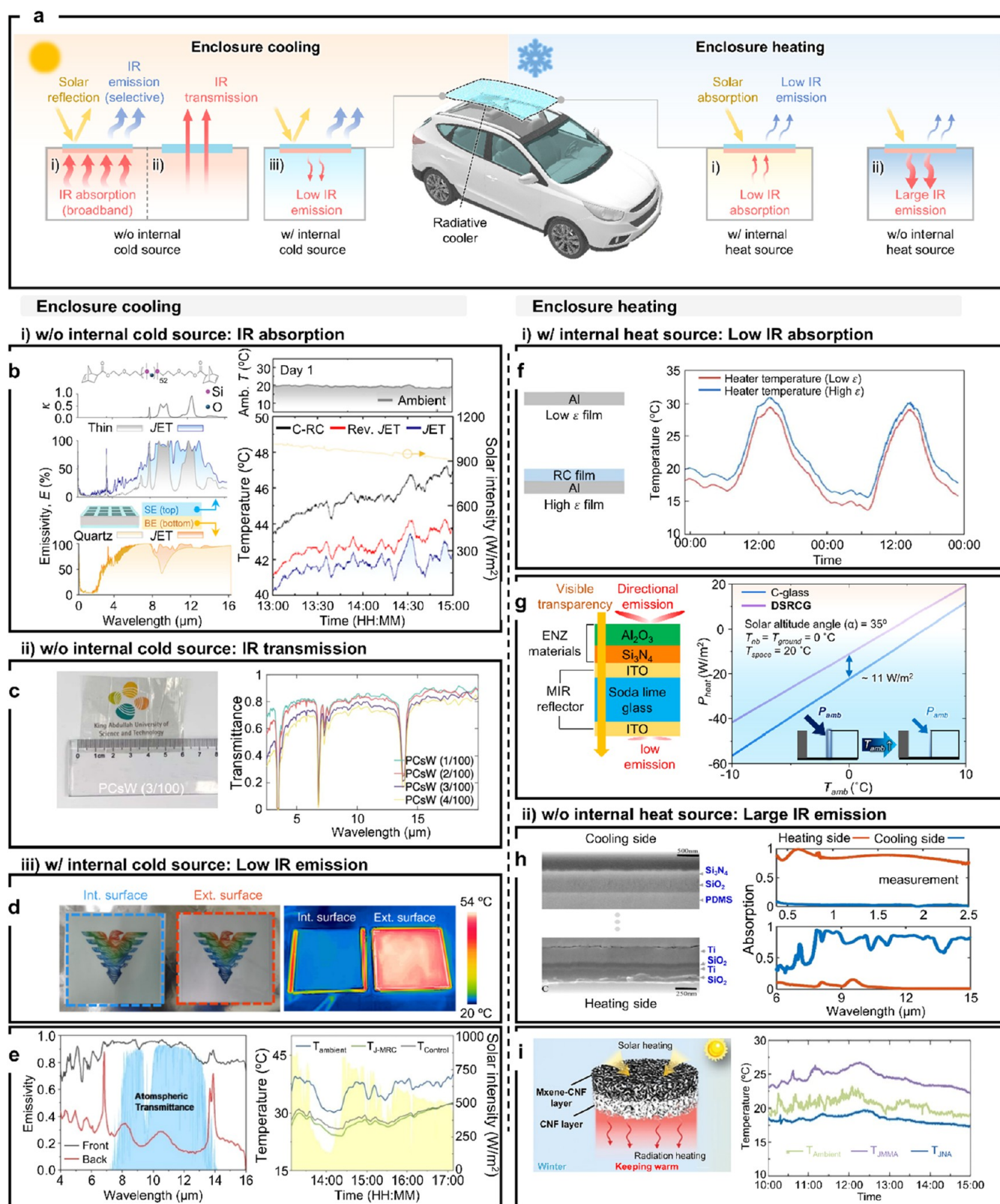


Figure 12. Thermal management methods for enclosures. (a) Schematic illustration of desirable thermal management methods under each condition. (b–e) Radiative coolers applicable for enclosure cooling. (b) The emissivity spectra of *Janus* emitter (JET) and the enclosure temperature measurement result of radiative objects. Adapted with permission from ref 405. Copyright 2020 AAAS. (c) The photograph of polyethylene (PE) film infused with cesium tungsten oxide (Cs_{0.33}WO₃) nanoparticles (PCsW cover) and MIR transmittance spectra depending on Cs_{0.33}WO₃ nanoparticles to PE weight ratio. Adapted with permission from ref 411. Copyright 2025 Elsevier. (d) The photograph and IR image of a pattern covered by interior (Int.) and exterior (Ext.) surface of enhanced color-preserving radiative cooling (ECRC) strategy. Adapted with permission from ref 262. Available under CC BY 4.0 license. (e) The IR emissivity spectra of the radiative cooling film with *Janus* optical properties (J-MRC) and the result of the enclosure temperature measurement. Adapted with permission from ref 415. Available under CC BY 4.0 license. (f–i) Thermal regulators applicable for

Figure 12. continued

enclosure heating. (f) The schematics of the low-emissivity (low ϵ) and high-emissivity (high ϵ) films and the measured temperatures of the heaters in the experimental setups. Adapted with permission from ref 416. Copyright 2023 Elsevier. (g) The schematic of dual-sided radiative cooling glass (DSRCG) structure and the calculated power transferred to the enclosure (P_{heat}) under winter urban conditions. Adapted with permission from ref 417. Available under CC BY 4.0 license. (h) The structure and the absorption spectra of the *Janus* multilayer. Adapted with permission from ref 418. Copyright 2021 American Chemical Society. (i) The schematic of *Janus* structured MXene-nanofibrils aerogel (JMNA) and the result of enclosure temperature measurement. Adapted with permission from ref 419. Copyright 2023 John Wiley and Sons.

the outer surfaces (e.g., wall, roof, and window) of enclosures, including vehicles,^{47,389–391} buildings,^{164,313,392,393} greenhouses,^{394–396} and spacecraft.¹⁴⁴ Meanwhile, several groups have developed solar absorbers with minimal IR emission to provide enclosure heating in winter or at nighttime.^{313,397,398} For year-round thermal regulation, recent works also have proposed radiative coolers for adaptive thermal control, whose optical properties can be properly adjusted (i.e., solar absorptivity and IR emissivity) in response to surrounding temperatures.^{334,371,399}

Specifically, the enclosure temperature is strongly affected by the temperature and optical properties of the inner surface.⁴⁰⁰ In particular, the desired IR emission property of the inner surface for efficient enclosure cooling depends on the relations between the indoor and outdoor temperatures of the enclosure and its surfaces. Additionally, the impact of the inner surface becomes more important under several practical conditions, such as a limited sky-view factor (SVF) (e.g., urban areas)^{401,402} and a high convective heat transfer coefficient (i.e., windy conditions).⁴⁰³ Under these cases, the enclosure cooling performance can be further enhanced by incorporating inner-surface IR control, rather than utilizing a single-sided emitter alone. In summertime, the enclosure is typically cooler than the outer surface, and low wall thermal resistance causes heat conduction into the enclosure, hindering temperature regulation.⁴⁰⁴ In this case, the inner surface exhibiting a low emissivity is suitable for minimizing heat radiation into the enclosure. Accordingly, this section highlights the suitable IR emission properties of the inner surface required for ideal thermal regulation under various conditions, along with the notable strategies to achieve these properties. Figure 12a summarizes the desirable IR emission properties of the inner surface depending on the presence of internal cold and heat sources. Without an internal cold source (e.g., air conditioner and water chiller), a significant amount of heat can be accumulated in the enclosure, remarkably increasing the enclosure temperature. This is because the windows and films of enclosures transmit the incoming solar radiation, while the windows and inner walls are opaque to outgoing IR emission from interior objects. Such heat accumulation can be mitigated by designing the inner surface to (i) absorb IR emission from the enclosure or (ii) transmit the emission directly to the outdoors. However, if the enclosure is cooled by an internal cold source, these strategies may instead induce unwanted IR emission from the comparably hot inner surface to the enclosure. This phenomenon can degrade the cooling performance as well as increase cooling energy consumption. Thus, (iii) minimizing the IR emissivity of the inner surface can suppress undesirable heat emission to the enclosure, facilitating the enclosure temperature control. Similarly, tailoring the emission properties of the inner surface can also improve enclosure heating performance. When an internal heat source is operating, the enclosure temperature becomes sufficiently higher than the cold ambient. Thus, (i) minimizing heat absorption to the inner surface prevents heat loss of the enclosure. On the other hand, without an internal heat

source, the enclosure can be cooled to a temperature similar to the ambient. Therefore, (ii) designing the inner surfaces to exhibit high IR emissivity promotes heat supply to the enclosure, raising its temperature.

As shown in Figure 12b, Heo et al. proposed a *Janus* emitter (JET) whose bottom side absorbs heat from the enclosure within a broadband IR range while the top side selectively emits heat within the AW.⁴⁰⁵ The broadband emission of the bottom side was accomplished by integrating PDMS and quartz layers. On the other hand, the selective emission of the top side was realized via spoof surface plasmon polariton (sSPP) resonance induced by the Ag–PDMS layer on the micropatterned quartz substrate. Under direct sunlight, the enclosure temperature of the experimental setup with the JET was ~ 4 and ~ 1 °C cooler than the reverse-JET (Rev. JET) and conventional radiative cooler (C-RC), respectively. The experimental result indicates that the strategy of drawing heat from an enclosure can be an effective way to cool a comparably hot enclosure. Moreover, lowering the thermal resistance of emitters could be a promising strategy to further facilitate heat transfer to the outdoor environment and enhance the enclosure cooling performance.^{406–410}

For greenhouses, the cover is required to allow high transmission in photosynthetically active radiation (PAR; 0.4–0.7 μm) for sufficient plant growth. The cover should also prevent solar-induced overheating by minimizing near-infrared (NIR; 0.7–2.5 μm) transmission. In addition, especially when highly emissive objects such as soil and leaves are present inside, a film with high IR transmittance can improve enclosure cooling.^{411,412} Tian et al. recently suggested a solution for passive greenhouse cooling by combining a spectrally selective cover (PCsW cover) with a cellulose ground mulch (Figure 12c).⁴¹² The PCsW cover is composed of polyethylene (PE) film infused with cesium tungsten oxide ($\text{Cs}_{0.33}\text{WO}_3$) nanoparticles. The PE film exhibits high solar transmittance ($>90\%$) while $\text{Cs}_{0.33}\text{WO}_3$ nanoparticles provide NIR absorption property induced by the small polaron effect.⁴¹³ Therefore, the PCsW cover effectively blocks unnecessary incoming near-infrared sunlight and prevents excessive solar heating. Especially, the PCsW cover with a $\text{Cs}_{0.33}\text{WO}_3$ weight ratio of 3/100 (3%) maintains its PAR transmittance at 73%, while its NIR transmittance decreases to 50%. Considering that the PAR transmittance of $\sim 70\%$ is regarded as a sufficient value for seedling growth,⁴¹⁴ the PCsW cover is expected to transmit enough PAR to sustain plant growth. On the other hand, the cover maintains a high MIR transmittance (0.73), facilitating efficient heat dissipation by transmitting the IR emission from the cellulose ground mulch, which features a high MIR emissivity (0.92). Although the solar reflectivity of the cellulose mulch (0.93) is similar to that of the aluminized mulch (0.89), the integration of the PCsW cover with the cellulose mulch showed a maximum enclosure temperature reduction of 14.7 °C, compared to the integration of a sunshine board with an aluminized mulch. Since the PCsW cover has ~ 0.72 higher MIR

transmittance compared to the aluminized mulch, the result confirms that transmitting IR emission from interior objects can be an advantageous strategy for passive greenhouse cooling.

As previously mentioned, the enclosures can maintain cool conditions by operating cooling systems such as air conditioners during summer. In this case, reducing the IR emission from the inner surface provides a beneficial approach for enclosure temperature control. Zhu et al. designed an enhanced color-preserving radiative cooling (ECRC) strategy to lower the cooling energy consumption of an actively temperature-regulated enclosure (Figure 12d).²⁶² Both the exterior (Ext.) and interior (Int.) surfaces of the ECRC strategy utilize visibly transparent materials to preserve the aesthetics of buildings. Simultaneously, their contrasting MIR emission properties maximize enclosure cooling performance. The Ext. surface, composed of 30 layers of TiO_2 and SiO_2 , exhibits high MIR emissivity (0.88). On the other hand, the Int. surface employs an ITO film as a radiant barrier, featuring a low MIR emissivity (0.21) and minimizing the heat emission to the enclosure. With an internal thermoelectric cooler, the enclosure temperature of the roof with ECRC was 9.6 and 3.6 °C lower than those of the bare roof and the roof with only a hot mirror (i.e., with only the Ext. surface of the ECRC), respectively. Furthermore, the roof with ECRC reduced the cooling power consumption by up to 63% compared to the bare roof at a fixed enclosure temperature of ~26 °C. In 2024, Yang et al.⁴¹⁵ fabricated a radiative cooling film with *Janus* optical properties (*J*-MRC) (Figure 12e) and confirmed its enclosure cooling performance. The outer surface of *J*-MRC comprises a nano-PE film and a hot-pressed PEO film (HP-PEO), exhibiting strong emissions within the broadband MIR range. Meanwhile, the inner surface consists of a nano-PE film with low MIR emissivity and an AgNWs layer that thermally isolates the inner and outer surfaces. Specifically, when ~100 g of ice is installed as an internal cold source, the chamber with *J*-MRC was able to cool the enclosure temperature maximally 1.4 °C lower than that of the control group (outer surface of *J*-MRC). Such works indicate that the method involving a low-emissivity inner surface can be practical for cooling and energy saving in actively temperature-regulated enclosures.

Employing an inner surface with a low IR emissivity can also be advantageous for enclosure heating cases, especially when an internal heat source keeps the enclosure warm. The low-emissivity inner surface absorbs less heat from the enclosure compared with conventional building materials, thus reducing the heating demand of enclosures. Zhao et al. demonstrated the applicability of low-emissivity inner surface for minimizing heat loss of enclosures (Figure 12f).⁴¹⁶ They simply fabricated a low-emissivity (low ϵ) film with Al foil and a high-emissivity (high ϵ) film by depositing a polyethylene terephthalate (PET) layer onto Al foil. With an internal heater applied in the setup, the average nighttime heater temperature in the low ϵ case was 1.8 °C higher than that in the high ϵ case. In addition, the simulated heat loss of Beijing buildings in the low ϵ case showed a 33.2% reduction compared to that in the high ϵ case. Similarly, Kwak et al. designed dual-sided radiative cooling glass (DSRCG) incorporating a low-emissivity inner surface composed of an ITO layer (Figure 12g).⁴¹⁷ Under simulated winter urban conditions, the calculated power transferred from the glass to the enclosure (P_{heat}) of the DSRCG was ~11 W m⁻² higher than that of the soda-lime glass (C-glass). Moreover, the difference in P_{heat} between the two glasses increased as the ambient temperature (T_{amb}) dropped. These encouraging results demonstrate the possibility of a low-emissivity inner surface

for maintaining mild enclosure temperatures under cold outdoor conditions.

As mentioned already, when no internal heat source is operating, the enclosure temperature can decrease closely to cold ambient. To realize enclosure heating for such conditions, several studies have integrated solar absorbers to the outer surface and transferred the absorbed heat into the enclosure via inner surfaces with high IR emissivity. Wang et al. proposed an applicable method by fabricating a *Janus* multilayer including both heating and cooling sides (Figure 12h).⁴¹⁸ Enclosure heating can be achieved by orienting the heating and cooling sides as outer and inner surfaces, respectively. The cooling side, composed of Si_3N_4 , SiO_2 , PDMS, and an Ag layer, exhibits broadband IR emission and low solar absorption. Meanwhile, Ti and SiO_2 were integrated as the heating side to reduce IR absorptivity (i.e., emissivity) and increase solar absorptivity. As a result, the cooling side features solar and IR absorptivity of 0.04 and 0.66, respectively, whereas the heating side has corresponding values of 0.87 and 0.05. Another approach developed by Yang et al. is *Janus* structured MXene-nanofibrils aerogel (JMNA) featuring an asymmetric design (Figure 12i).⁴¹⁹ The outer MXene-CNF layer strongly absorbs sunlight and converts it into thermal energy while minimizing IR emission and heat loss. The generated heat is then transferred to the enclosure via the inner porous CNF layer with high IR emissivity. As a result, the enclosure temperature of the chamber with JMNA was ~6 and ~4 °C higher than those of the chamber with CNF aerogel (JNA) and ambient, respectively. The measurement results indicate that JMNA enables efficient heat transfer from the heated outer surface to the enclosure through the emissive inner surface.

Enclosure thermal regulation based on passive radiative cooling can facilitate enclosure temperature control as well as reduce cooling and heating energy consumption. Nevertheless, the studies applying radiative coolers to vehicles,^{47,389–391,405} greenhouses,^{394–396,411,412} and spacecraft^{144,399} remain relatively unexplored compared to building applications.^{164,262,313,334,392,393,397,398,415–419} In this section, several promising strategies for enclosure thermal regulation under various internal and external conditions are provided. These strategies present the potential of radiative cooling for broader applications in enclosure thermal regulation.

Manufacturing and cost drivers are important considerations for practical deployment. To reduce the production cost of emitters and facilitate large-scale production, it is essential to utilize cost-effective fabrication methods. The processes such as electrophoretic deposition of multilayer structures,⁴²⁰ phase transition method for porous structure,⁴²¹ and electrospinning to form fiber membrane²³¹ are promising technologies to reduce fabrication cost. Notably, the roll-to-roll method⁵² and paint-like facile fabrication⁷⁸ can offer production methods for large-scale surface coatings of outdoor structure exteriors.

Reliability and lifetime in real environments are also critical for real-world applications. The emitters should exhibit sufficient outdoor durability for applications in buildings or vehicles. Especially, the emitters are required to maintain their original structure and optical properties (e.g., high solar reflectance and infrared emissivity) under continuous UV exposure, weathering induced by rain or wind, and temperature cycling. In this context, hydrophobic coatings like 1H,1H,2H,2H-Perfluorodecyltriethoxysilane,⁴²² aluminum oxide nanoparticles,⁴²³ and a mixture of (heptadecafluoro-1,1,2,2-tetrahydrodecyl) trichlorosilane and hexane²⁸ can

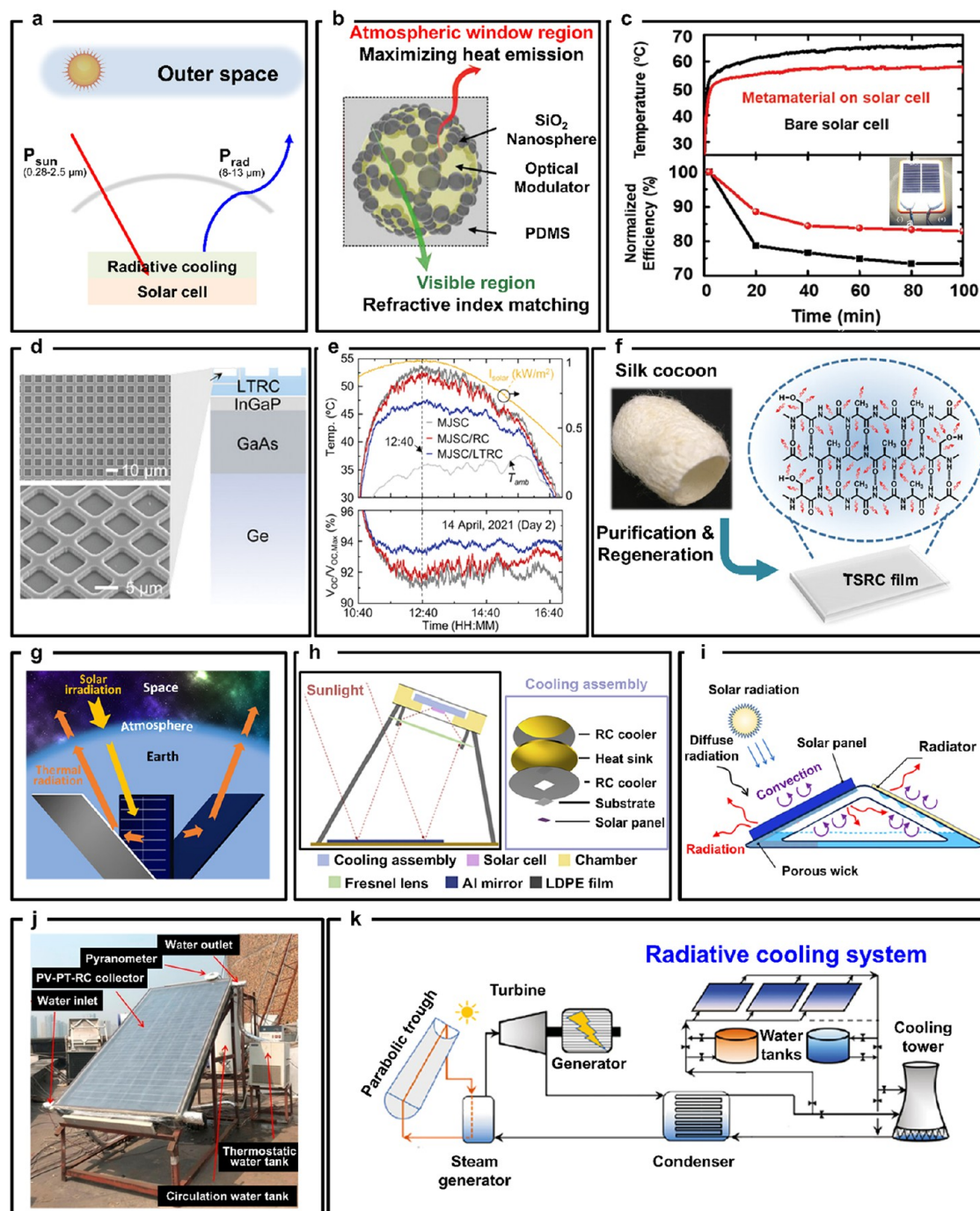


Figure 13. Various efforts to apply RC technology to high-performance solar energy systems. (a) Schematic diagram for the integration of RC and solar cells. Reproduced from ref 428. Available under a CC-BY 4.0 license. Copyright 2024 The Author(s). (b) Schematic illustration of the working principle and (c) RC performance of visibly clear RC metamaterials. Reproduced with permission from ref 34. Copyright 2021 Wiley-VCH. (d) Schematic diagram of multijunction solar cells with micrograting structures for light trapping and RC, and (e) their performance of outdoor field tests. Reproduced with permission from ref 444. Copyright 2021 Wiley-VCH. (f) Schematic illustration of the transformation of opaque cocoons into a transparent silk fibroin RC (TSRC) film. Reproduced with permission from ref 445. Copyright 2023 Wiley-VCH. (g) Schematic illustration of the working principle of v-PV system, which combines a V-shaped aluminum mirror and a vertical PV system. Reproduced from ref 280. Available under a CC-BY 4.0 license. Copyright 2024 Authors. (h) Schematic illustration of reverse concentrating PV panel for double-sided RC. Reproduced with permission from ref 352. Copyright 2020 Elsevier. (i) Schematic illustration of loop heat pipe integrated RC solar panel. Reproduced with permission from ref 446. Copyright 2024 Elsevier. (j) Photograph of a practical-scale photovoltaic/thermal collector installation. Reproduced with permission from ref 432. Copyright 2018 Elsevier. (k) Schematic diagram of a RC integrated solar thermal power plant. Reproduced from ref 434. Available under a CC-BY 4.0 license. Copyright 2022 The Author(s).

prevent emitters from rainwater erosion. Moreover, trimethylchlorosilane-modified inorganic SiO₂⁴²⁴ and mixed Al₂O₃ and TiO₂ nanoparticles⁴²³ can offer UV resistance to the emitters.

Application-specific barriers and representative solution pathways should also be considered. In particular, the high thermal resistance in the Janus emitter concept can hinder heat

removal from the enclosure and degrade enclosure cooling performance. Several research groups reduced the thermal resistance of emitters by incorporating thermally conductive materials such as hexagonal boron nitride (h-BN) nanoplates,⁴⁰⁶ nickel–titanium spring,⁴⁰⁷ graphene,^{409,410} or diamane nanosheets.⁴⁰⁸ These strategies can further facilitate heat removal from the enclosure and enhance the cooling performance.

In terms of deployment maturity, the reliability of thermal regulation performance and outdoor durability of the emitters have been validated at the laboratory scale. The manufacturing methods that enable scalable production have also been introduced by several research groups. Nevertheless, the cost-effective materials still need to be further explored, and emitters' compatibility with conventional building materials should be demonstrated for building and vehicle applications.

5.3. High-Performance Solar Energy System

Jung Bin Yang and Dong Rip Kim

Solar energy has emerged as one of the most promising energy sources to meet the growing global demand for environmentally friendly and renewable power generation.^{425–427} Considerable research has been conducted to improve the efficiency and performance of solar energy systems, including (concentrating) solar panels,^{34,280,428,429} the photovoltaic/thermal collector (PV–PT) systems,^{430–432} and concentrating solar thermal power (CSP).^{433–435} However, these systems face a common challenge: elevated operating temperatures caused by solar radiation absorption, which reduces energy conversion efficiency.^{425,426,434,436} Active cooling technologies, such as forced air cooling and liquid cooling, can effectively lower device temperature but require additional energy input, increasing operational costs and maintenance burdens.^{280,425} Passive cooling methods, such as natural convection cooling,^{437,438} integrated heat sinks,^{439,440} and phase change materials,⁴⁴¹ have been extensively studied. RC is emerging as a promising passive thermal management strategy for high-performance solar energy systems. RC works by directly emitting thermal radiation into cold outer space through the atmospheric transparency window (with a wavelength range of 8 to 13 μm), thereby significantly reducing the device temperature without additional energy input. This environmentally friendly and cost-effective approach offers significant potential for sustainable solar power generation. In this section, we present research on applying RC technology to solar energy systems. Specifically, we discuss integration strategies, system-level efficiency improvements, limitations, and future outlook.

Despite various efforts to improve RC performance, most RC materials have adopted opaque designs, such as white or silver coatings, which limit direct application to solar panels.⁴⁰ For integration with solar modules, RC materials must combine high transparency in the visible wavelengths of solar spectrum with strong emissivity in the MIR range (Figure 13a).⁴²⁸ To meet these criteria, researchers have explored strategies such as refractive index matching,^{34,131} multilayer architectures,^{56,442} and silica photonic crystal structures.^{40,147,443} For example, Lee et al.³⁴ successfully fabricated an RC metamaterial using PDMS, SiO_2 , and *n*-hexadecane, which have similar refractive indices and low extinction coefficients in the visible wavelength (Figure 13b). *n*-hexadecane infiltrated the micropores of the SiO_2 aerogel, acting as an optical modulator, resulting in excellent photonic cooling performance while remaining transparent. In addition, the high flexibility and scalability of the PDMS substrate further enhance its applicability to solar cells. To verify

the performance change due to RC of a solar cell, a commercial Si solar cell (efficiency 10.35%, open-circuit voltage 3.65 V, short-circuit current density 27.69 mA/cm^2) was subjected to light soaking using an AM 1.5G solar simulator as shown in Figure 13c. The metamaterial-covered solar cell suppressed the temperature increase by about 8.5 °C during 100 min of light absorption compared to the control cell, showing about 1.5 times lower degradation (The normalized efficiency decrease of the metamaterial-covered solar cell was 17%, while that of the control solar cell was 26%). Heo et al.⁴⁴⁴ analyzed the effectiveness of radiative coolers integrated with various types of solar cells and demonstrated that multijunction solar cells (MJSC, InGaP/GaAs/Ge) benefited most from RC due to their higher temperature-efficiency sensitivity. They designed and fabricated a light-trapping radiative cooler (LTRC) using micrograting of quartz and integrated it into MJSC as shown in Figure 13d. As a result, the MJSC/LTRC exhibited a near-unity thermal emission in the long-wave infrared region, enhancing solar energy gain across the solar spectrum. Outdoor field tests (solar irradiation of $\sim 900 \text{ W m}^{-2}$) experimentally demonstrated that the MJSC/LTRC effectively suppressed the temperature increase of the cell by ~ 6.1 °C, while enhancing photon absorption due to the light trapping effect and minimizing open-circuit voltage degradation (2% increase of $V_{\text{OC}}/V_{\text{OC,max}}$ compared to the control sample) as shown in Figure 13e. Chen et al.⁴⁴⁵ developed a transparent silk radiative cooling (TSRC) film and applied it to the solar panel. During the purification/regeneration process of silk (*Bombyx mori*), the fibrous morphology was transformed and the secondary structure of silk fibroin protein was disrupted to improve transparency in visible wavelengths, while securing high broadband emissivity in the MIR region by maintaining the molecular structure of the backbone and side chains (Figure 13f). Sericin, which adversely affected adhesion to substrate, was removed during the purification process, resulting in effective adhesion to commercial poly-Si solar panels. The performance of the TSRC-coated solar panels was investigated in an outdoor environment of $\sim 900 \text{ W m}^{-2}$. The steady-state temperature of the TSRC film-coated solar panel (61 °C) was 14 °C lower than that of the bare panel (75 °C). This improved the open circuit voltage of the solar panel from 5.7 V (Bare) to 6.0 V (TSRC film-coated), resulting in a 7% improvement in solar cell efficiency of the TSRC film-coated solar panel (9.52%) compared to the bare one (8.91%).

In addition, RC can be implemented through indirect cooling designs.^{280,352,431} In typical monofacial PV modules, deploying RC onto the rear-side of PV modules can be ineffective because the temperature difference between the backside and the ground is small, reducing net radiative heat flux. For example, when the temperature of the PV module (assumed to be a blackbody) is 323 K, the net radiative heat flux using a 300 K ground heat sink was about 60% of the heat flux using a zenith heat sink.²⁸⁰ To solve this problem, Fang et al.²⁸⁰ proposed a V-shaped PV (v-PV) system combining a vertical PV module with aluminum mirrors to reflect and radiate rear-side emissions to the sky (Figure 13g). They optimized the angle between the panel and the mirror through simulations to improve the solar irradiance and RC efficiency (modified v-PV). Outdoor test (Thuwal, Saudi Arabia, on Nov. 13, 2022) showed that the modified v-PV increased average irradiance by $\sim 15\%$ (1065 W m^{-2}) and maximum power output by $\sim 17\%$ (5.77 W) compared to the control (modified h-PV, 929 W m^{-2} and 4.94 W). They also predicted that their proposed design would have a lower

degradation rate (reduction of 0.043%/year) and LCOE (levelized cost of energy) of 0.3411 USD/kWh (13% reduced compared to the bare one) by lowering the temperature and increasing the power output. Wang et al.³⁵² integrated a heat sink on the rear of a concentrating photovoltaic (CPV) cell and applied soda-lime glass radiative coolers to both the front and back surfaces (Figure 13h). They also used aluminum reflectors to reverse the CPV panel so that the back side faced the zenith, which enabled double-sided RC. They verified the cooling performance with and without the radiative cooler through outdoor tests (direct normal irradiance of 1019 W m⁻²). As a result, they confirmed that the presence of the cooler resulted in a temperature of up to 36 °C lower than that without it, which led to a significant increase (27%) in the open-circuit voltage. Hamdan et al.⁴⁴⁶ combined RC with a loop heat pipe (LHP) system (Figure 13i), transferring heat from the sun-facing surface to a shaded RC surface through the LHP, and the radiative cooler then dissipates the heat load to the sky. They numerically verified that their proposed LHP RC system can reduce the maximum temperature by more than 10 °C (weather for June 1, 2022 in Sharjah, United Arab Emirates) and improve the electrical efficiency by 4.6% compared to the control (without LHP and radiator), and such a system can achieve an annual energy saving of 8.7 kWh/m².

Meanwhile, in addition to solar panels, various solar energy systems require various cooling loads. In this regard, RC is one of the attractive strategies for achieving high-efficiency solar energy systems using passive methods.^{431–435} PV–PT is a system that can simultaneously produce thermal and electrical energy by converting solar energy into usable forms, which draws much attention for its high overall efficiency and dual function by extracting the excess heat of PV modules.⁴³⁰ Specifically, the integration of RC can further highlight the advantages of PV–PT systems by adding a night-time cooling function. They can not only generate electricity, but also provide hot water, cooling, and heating, which is attractive in building energy management.⁴³⁰ Hu et al.⁴³² designed and fabricated a practical-scale PV–PT–RC collector (total area 1.12 m² with 72 monocrystalline silicon solar cells) and systematically analyzed its electricity generation, heating, and cooling performance through outdoor experiments (Figure 13j). Their experimental results showed that the electrical efficiency of the PV–PT–RC collector in daily system mode was 9.69–11.7%, the RC power on a clear night was 72 W m⁻², and the total cooling energy gain of the PV–PT–RC system was reported to be 2.9 MJ in night-time operation. In CSP plants, wet cooling is widely used to condense steam and maintain high turbine power conversion efficiency, but water scarcity limits its application in arid, high-irradiance regions.^{434,435} In one innovative approach, Ali et al.⁴³⁴ integrated RC into the precooling to reduce the cooling load on the cooling tower of the CSP system (Figure 13k). Specifically, using the Mojave Solar Project's CSP solar plant (280 MW) as a reference power generation and the National Solar Irradiance Database (NSRDB) weather data of 3000 locations in the contiguous U.S., the performance of an RC-integrated CSP plant was numerically analyzed. As a result, they confirmed that for the southwestern U.S. region, a suggested RC-integrated CSP system could save 65 to 85% of water compared to the conventional system. However, they found that the evaluated cost of this technology is \$55 to 110 per kW, which was significantly higher than that of conventional alternatives. Therefore, further investigation is needed to explore high-performance and low-cost RC technologies that can reduce this cost. Zeyghami et al.⁴³³

proposed the integration of RC to an air-cooled CSP plant to reduce its cooling load. The RC system was added between the air cooling and the main compressor both in the simple and recompression supercritical carbon dioxide (CO₂) cycle, thereby further reducing the fluid temperature entering the compressor. This allowed the RC system to decrease the cooling load, improving overall cycle performance. Consequently, for the recompression supercritical CO₂ cycle operating at a maximum temperature of 550 °C, the net output power increased by 7.5%, when using 18.26 m²/kW_e of RC.

Despite the progress in RC integration strategies for high-performance solar energy systems, several challenges remain for future research. First, large-scale system-level integrated performance analysis through outdoor experiments is necessary. Existing studies, with a few exceptions,⁴³² have been limited to the cell level.^{34,280,445} In addition, comprehensive outdoor field tests under real-world conditions are necessary to verify the performance enhancement of RC, since high humidity can significantly degrade RC performance and cloudy days can adversely affect the performance of solar energy systems.⁴²⁶ Therefore, comparing performance under various outdoor conditions will provide valuable insights into practical application considerations. From this perspective, large-scale application of RC technology and performance verification through outdoor experiments will increase the feasibility of its practical application in high-performance solar energy systems. Second, the development of novel materials and manufacturing that achieve high RC performance at lower costs is necessary. While numerous studies have demonstrated high-performance RC properties, reports that also consider cost are limited.^{426,427} Despite its high performance of RC, cost remains a major obstacle to its practical application. Therefore, significant progress in cost reduction can make RC technology an attractive option for solar energy devices. Furthermore, research is needed on the manufacturing side for applying those materials to complex geometries or large-area applications. In summary, high-performance RC research that considers cost, materials, and applicability (manufacturing) is necessary. Finally, durability research is essential. All solar energy systems are operating outdoors, suggesting the necessity of long-term durability tests under various climatic conditions, such as UV-induced degradation, thermal cycling-induced aging, dust accumulation-induced performance degradation, and corrosion. Addressing these challenges through large-scale outdoor tests, low-cost material development, and durability studies will be key to realizing the full potential of RC in advancing global renewable energy goals.

From a deployment perspective, several additional practical considerations should also be noted. Manufacturing and cost drivers are important considerations for PV-related RC integration. The main cost drivers of direct PV integration are the integration of transparent RC layers with simultaneous high solar transmittance and strong MIR emissivity,^{34,428,444,445} whereas indirect RC–PV/CPV systems shift cost toward auxiliary devices such as mirrors, heat sinks, loop heat pipes, and cooling towers.^{280,352,434,446} Reliability and lifetime in real environments are also critical, as all target systems operate outdoors. Their lifetime will depend on resistance to UV exposure, thermal cycling, humidity, dust/soiling, corrosion, and retention of optical selectivity over time.^{426,427} At the same time, several application-specific barriers remain. The main barriers are the transparency-cooling trade-off in front-side PV integration, limited sky access for conventional rear-side PV

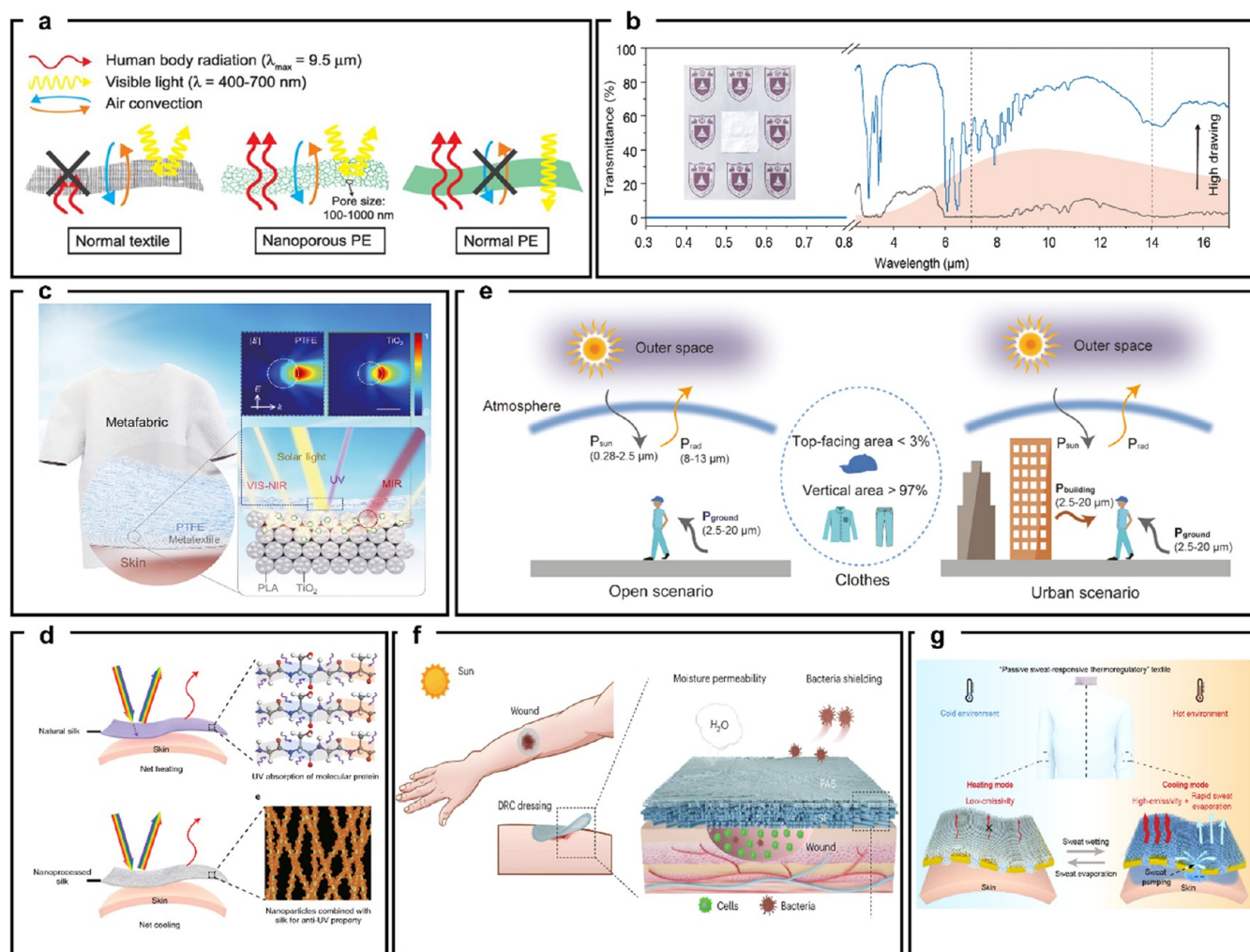


Figure 14. Radiative cooling applications for personal thermal management. (a) Schematics of comparison between nanoPE, normal PE, and cotton. Reproduced with permission from ref 176. Copyright 2016 The American Association for the Advancement of Science. (b) The total transmittance of infrared and visible light for the IRT-PA6 textiles (blue curves) and the IR transmittance of drop-casting films (gray curves) that are obtained from the volatilization of spinning solution. Reproduced from ref 456. Available under a CC-BY license. Copyright 2025 The Author(s). (c) Schematic of a metafabric for daytime radiative cooling. Adapted with permission from ref 457. Copyright 2021 The American Association for the Advancement of Science. (d) Subambient daytime radiative cooling design for nanoprocessed silk. Reproduced from ref 458. Available under a CC-BY license. Copyright 2021 The Author(s). (e) Schematic of wearable fabrics in an open scenario and an urban scenario. Adapted with permission from ref 239. Copyright 2024 The American Association for the Advancement of Science. (f) Schematic of the structural design of daytime RC dressings for local wound environment management under sunlight. Reproduced from ref 459. Available under a CC-BY license. Copyright 2024 The Author(s). (g) The PSRT textile maintains human body temperature stability in a dynamic environment with temperature variations. Reproduced from ref 460. Copyright 2025 American Chemical Society.

layouts, the scarcity of system-level outdoor validation, and the high added cost of RC hardware in CSP integration.^{280,426,432–434} Several representative solution pathways have been proposed to address these barriers. Promising pathways include transparent index-matched or structured RC coatings for front-side integration,³⁴ V-shaped or double-sided sky-coupled PV/CPV configurations,²⁸⁰ remote radiators assisted by loop heat pipes,⁴⁴⁶ and hybrid PV–PT/CSP design where RC is integrated at the subsystem level.^{432,434} In terms of deployment maturity, transparent PV coating/film integration remains at the prototype or limited outdoor validation stage, while microstructure-assisted PV/CPV systems are still at the early engineering prototype stage. By comparison, PV–PT-RC has reached practical-scale field demonstration, whereas CSP integration remains largely at the simulation and technoeconomic stage.

5.4. Personal Thermal Management

Yansu Hou and Jia Zhu

Over the past few decades, greenhouse gas emissions have accelerated global warming.^{447,448} High summer temperatures pose a serious threat to human health, leading to heat-induced illnesses and related complications such as heatstroke, skin cancer, and cardiovascular diseases.⁴⁴⁹ Therefore, the development of personal cooling technologies has become particularly important and has attracted extensive attention and research efforts in recent years. Specifically, radiative cooling fabrics optimize the thermal exchange pathways between the human body, the fabric, and the environment through optical regulation of emission, transmission, and reflection, thereby achieving passive all-day cooling without any additional energy input.⁴⁵⁰

Existing radiative cooling fabrics can be classified into three distinct types based on their thermal management mechanisms.

The first type is transmission-type fabrics, which optimize high infrared transmission within the human body's radiation bands, establishing efficient thermal radiation channels to enhance heat dissipation from the body surface, primarily for indoor environments.^{176,451} The second type is emission-type fabrics, which enhance solar reflectivity to inhibit external heat gain, along with high mid-infrared emissivity to promote radiative cooling.^{452,453} The third type is selective emission/transmissive fabric that employs precise spectral design to achieve high emissivity in atmospheric windows and high transmissivity in nonatmospheric windows, thereby enabling all-weather thermal comfort regulation.^{205,454,455}

Due to the fundamental differences between indoor and outdoor application scenarios, extensive research has been devoted to exploring this distinction. Indoor cooling fabrics depend on high infrared radiation transmission to reduce heat buildup and promote cooling. Intrinsic MIR transparent materials are not common, Hsu et al. demonstrated nanoporous polyethylene (nanoPE) as a novel candidate material for human body radiative cooling (Figure 14a). Nanoscale pores ranging from 50 to 1000 nm are embedded in the polyethylene film, strongly scattering visible light while the mismatch with the mid-infrared wavelength range ensures that mid-infrared transparency is not compromised.¹⁷⁶ Furthermore, Chen et al. designed an infrared-transparent PA6 textile based on the common polymer nylon-6 (PA6) by employing a high-stretching process combined with rapid solvent evaporation (Figure 14b). By altering the chain conformation and crystalline structure, the molecular vibrations (infrared absorption) of PA6 in the infrared region were significantly weakened. Meanwhile, this process reduced the fiber diameter to the nanoscale and minimized infrared reflection. Compared with cotton textiles, the PA6 fabric achieved a cooling effect of up to 2.1 °C, corresponding to an estimated ~20% reduction in the energy required for indoor cooling.⁴⁵⁶

By contrast, outdoor radiative cooling fabrics require high solar reflectance and the ability to strongly absorb and emit human heat. By minimizing the solar heat absorption and maximizing the emission of heat from the human body to the environment, textiles can cool the human body even under intense solar exposure. Zeng et al. developed a metamaterial fabric with a hierarchical morphological structure, achieving a high solar reflectance of 92.4% in the solar spectrum and a high emissivity of 94.5% within the atmospheric window (Figure 14c).⁴⁵⁷ Through scalable industrial textile manufacturing routes, the fabric maintains efficient radiative cooling performance while exhibiting excellent mechanical strength, water resistance, and breathability required for commercial apparel. Practical application tests demonstrated that when covered with this metamaterial fabric, the human body temperature was approximately 4.8 °C lower than when covered with commercial cotton fabric. To achieve the radiative cooling effect, nanostructures are required. Unlike the design of the aforementioned metamaterial cooling fabric, Zhu et al. realized daytime radiative cooling below ambient temperature based on textiles (silk) (Figure 14d). Due to the inherent absorption of proteins in the ultraviolet region, natural silk is prevented from achieving net cooling under sunlight. This study explored the nanoprocessing of silk through molecular bonding design and scalable coupling agent-assisted dip-coating methods. Results demonstrated that the simulated skin temperature covered with nanoprocessed silk was reduced by 8 °C compared to natural silk. Furthermore, the study provided a comprehensive

evaluation of the impacts of nanoprocessing on human comfort. The nanoprocessed silk exhibited a water vapor transmission rate (WVTR) comparable to that of natural silk and commercial Tyvek, even slightly outperforming cotton. Regarding the wicking rate—a critical measure of moisture transport—the silk maintained excellent hydrophilicity with a wicking distance of 10 mm, significantly superior to the hydrophobic Tyvek, which lacks wicking capability entirely. Additionally, by employing a single-sided screen-printing technique to coat nanoparticles exclusively on the outer surface of the fabric, the inherent “cool-to-touch” tactile property of silk was preserved, while ensuring robust durability to endure 50 cycles of accelerated washing and drying. This research further provides a customizable strategy for the convenient and scalable design of natural materials.⁴⁵⁸ Most radiative cooling textiles are often designed as broadband emitters in the entire MIR region, without considering heat from the heated ground and urban buildings. Wu et al. designed a mid-infrared spectrally selective hierarchical textile (SSHF) (Figure 14e), achieving high emission in the AW, while high reflection in the non-AW to suppress parasitic heat from the ground or buildings.²³⁹ The rational optical design and fiber nanofabrication enable substantial cooling effects: The SSHF is 2.3 °C cooler than the broadband emitter when placed vertically and 6.2 °C cooler than the ambient temperature when placed horizontally. This spectrally selective design for vertically oriented fabrics offers an innovative solution to tackling urban heat islands.

Currently, much research is focused on developing radiative cooling textiles that can operate effectively under various environmental conditions and possess additional functionalities. Example include antimicrobial radiative cooling textiles that protect wounds under sunlight. Zhang et al. demonstrated a daytime radiative cooling dressing based on a polyamide 6/silk fibroin bilayer structure (Figure 14f), which can reduce the thermal load on skin wounds under sunlight exposure.⁴⁵⁹ Polyamide 6 with mid-infrared transparency and silk fibroin with biocompatibility jointly endow the dressing with a high mid-infrared emissivity (about 0.94) and solar reflectance (about 0.96), thus its temperature can be about 7 °C lower than the ambient temperature under direct sunlight. Under sunlight, this dressing can accelerate the wound healing rate. Furthermore, to address the challenges posed by fluctuating temperatures, such as substantial day-to-night variations, people have developed active and passive thermal-regulating textiles. For example, a sweat-responsive thermal-regulating textile based on unidirectional moisture wicking has been developed that can regulate mid-infrared radiation and sweat evaporation while remaining wearable to achieve the widest thermal comfort range (8.3–33.0 °C) currently available in dynamic environments (Figure 14g).⁴⁶⁰

From a commercialization perspective, the transition of RC textiles from laboratory prototypes to commercial products hinges on scalable manufacturing and cost-effective strategies. Current research demonstrates compatibility with industrial processes through techniques like coupling agent-assisted dip-coating, single-sided screen-printing, and high-throughput fiber drawing. By utilizing low-cost polymers like PA6 or natural materials (silk, cotton, and wood), additional material overhead is minimized. Environmental reliability is a critical benchmark; for instance, nanoprocessed silk has proven to maintain its optical and cooling performance through 50 cycles of accelerated washing and drying while preserving mechanical strength and breathability. To overcome application-specific

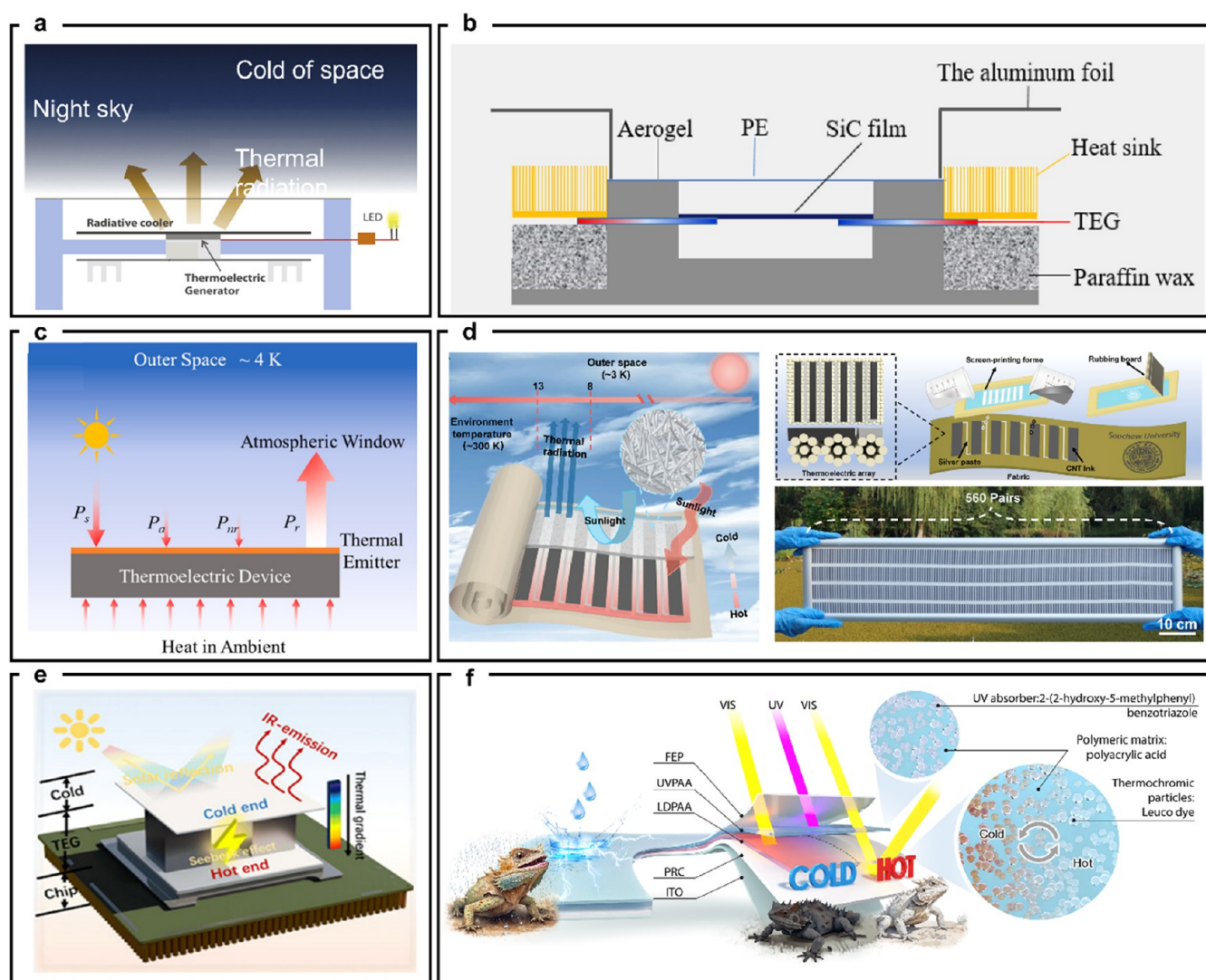


Figure 15. Radiative cooling applications for boosting electricity generation via thermoelectric systems. (a) Schematic of the nighttime thermoelectric system. Reproduced with permission from ref 347. Copyright 2019 Elsevier. (b) Main view of the structural scheme of the designed thermoelectric generator. Reproduced with permission from ref 475. Copyright 2020 Elsevier. (c) Schematic of TEG working mechanism based on radiative cooling. Reproduced with permission from ref 477. Copyright 2018 Elsevier. (d) Principle and the structures of wearable thermoelectrical device, schematic diagram of screen-printing process, and display of large-area fabric. Reproduced with permission from ref 478. Copyright 2025 The American Association for the Advancement of Science. (e) Principle and structure of B-TEG. Reproduced with permission from ref 479. Copyright 2025 John Wiley and Sons. (f) Design of bioinspired all-weather energy harvesting metafilms. Adapted with permission from ref 480. Copyright 2025 The American Association for the Advancement of Science.

barriers, such as parasitic heat from urban buildings, spectrally selective designs (e.g., SSHF) offer a solution by suppressing nonatmospheric window absorption. Furthermore, specialized solution pathways like antimicrobial bilayer dressings are expanding RC technology into healthcare. While the deployment maturity is supported by a solid theoretical foundation in material design, achieving a complete industrial value chain requires the coordinated optimization of visual aesthetics, washability, and thermal comfort to meet diverse market demands.

In summary, although radiative cooling fabrics have achieved foundational advances in material design principles that laid a solid theoretical basis, their successful commercialization still requires coordinated optimization of breathability, moisture permeability, washability, visual aesthetics, and thermal performance. Future directions will focus on advancing technological innovation in materials science, integrating

multifunctional systems, broadening cross-disciplinary applications, promoting environmental sustainability, and responding to evolving market demands. In addition, sustainable cooling fabrics can contribute to the low-carbon transformation of the textile industry. Natural materials like bamboo, wood, cotton, and linen can be used to design and develop environmentally friendly cooling fabrics. By innovating materials, advancing equipment technology, and strengthening industry standards, radiative cooling fabrics are expected to evolve into products with complete industrial value chains in the future.

5.5. Electricity Generation

Yansu Hou and Bin Zhu

The current fossil fuel-dominated power sector accounts for nearly 40% of global annual energy-related CO₂ emissions.⁴⁶¹ The low-carbon transition of the power sector is crucial to tackling climate change and ensuring the future supply of

energy.^{462,463} Traditional power generation methods, mainly relying on fossil fuels and even including some renewable energy sources such as solar and wind power,^{464,465} are facing severe challenges: Fossil fuel power plants account for about 30% of global carbon dioxide emissions, solar photovoltaic systems experience efficiency decline in high temperatures (for every 1 °C increase above 25 °C, efficiency drops by 0.4–0.5%),⁴⁶⁶ and wind turbines' operation depends on unstable weather conditions.⁴⁶⁷ To overcome these limitations, researchers are exploring innovative technologies that can enhance the sustainability and efficiency of power generation. Unlike active cooling methods that consume electricity, such as air conditioning or liquid cooling, radiative cooling utilizes the natural thermal radiation of materials to reduce heat accumulation, providing unique advantages for optimizing power generation systems.

TEGs are attractive as an environmentally clean technology for converting waste heat into electrical power through the Seebeck effect. Its advantages include minimal mechanical vibration, high scalability, and a long lifespan.⁴⁶⁸ The output power of the TEG is directly proportional to the temperature difference between its cold and hot ends.⁴⁶⁹ Therefore, researchers focus on methods to decrease the cold end temperature or raise the hot end temperature. However, TEG's efficiency is often limited by the temperature gradient between the hot end (exposed to waste heat) and the cold end (in contact with the ambient environment). The traditional cooling techniques involve installing air⁴⁷⁰ or water cooling devices⁴⁷¹ at the cold end of the TEG, but these methods require additional energy input, which will reduce the overall efficiency of the TEG. Therefore, people are seeking a passive cooling method to increase the output power of TEGs without affecting their efficiency.³⁴⁸

In 2019, Raman et al. constructed a thermoelectric system (TES) driven by RC.³⁴⁷ By radiating heat to the cold cosmic space, the radiative cooling technology maintains the cold end of the TEG below the ambient temperature (Figure 15a). The hot end is heated by the surrounding air. The temperature difference generates usable electrical energy. Their experimental findings demonstrated that the device could generate 25 mW m⁻² of power. This demonstration shows that the device can directly power a light-emitting diode, effectively generating light from the darkness of space itself. Subsequently, many researchers also proposed many TEGs driven by radiative cooling.^{472–474} However, due to the lack of strict spectral regulation of the cold end coating, the operation of the equipment was limited to nighttime. Xia et al. were the first to propose a fully weather-protected continuous electricity and water production device (Figure 15b).⁴⁷⁵ During the day, it absorbs solar radiation, and at night, it utilizes radiation cooling. The top part acts as the hot end during the day and the cold end at night. The opposite temperature gradient during the day and night causes the reversal of the output of the positive and negative electrodes. With the rapid development of micronano manufacturing technology, various kinds of photonic devices emerged,^{149,234,476} which have strict selectivity for electromagnetic wave in the region of 8–13 μm but strong thermal emission, thus effectively reflecting almost all incident sunlight. Therefore, they have been developed for daytime radiative cooling. Mu et al. have developed the first prototype of TEG utilizing RC that combines the ultrathin TEG with the thermal emitter (Figure 15c).⁴⁷⁷ The TEG-RC using SiO₂/Si₃N₄ alternating layer thermal emitters as radiative coolers (emissivity

up to 80.8%). They observed maximum temperature drop of 4 K was achieved by using the thermal emitter. The output voltage of the TEG-RC reached up to 0.5 mV, and the TEG-RC exhibited a continuous average 0.18 mV output more than 24 h.

In addition to developing high-efficiency TEG prototypes based on radiative cooling, Liu et al. integrated this concept into wearable thermoelectric textiles (Figure 15d).⁴⁷⁸ They screen-printed large-area carbon nanotube (CNT)-based thermoelectric arrays onto conventional fabrics, which were then combined with electrospun poly(vinylidene fluoride-co-hexafluoropropylene) (PVDF-HFP) films serving as radiative modulation layers. The resulting thermoelectric fabric (0.2 m²) achieves a substantial ΔT of 37 K under a solar intensity of ~800 W per square meter, yielding a peak power density of 0.20 milliwatt per square meter. Shi et al. integrated a fully biomass-based radiative cooling material into a thermoelectric device with a gradient structure (Figure 15e).⁴⁷⁹ The device achieved a power density of 7.61 W m⁻² under a temperature difference of $\Delta T = 30$ °C by harvesting waste heat from electronic components. This study provides an innovative approach for carbon-neutral cooling and sustainable energy applications.

The different demands for radiative cooling during day and night provide a direction for exploring how to achieve the switching of the spectral characteristics of cooling materials with the lowest energy consumption or in a completely passive manner. Optimizing the geometric characteristics of the thermoelectric system (especially the areas of the radiative cooler, solar absorber, and thermoelectric generator (TEG)), and integrating the passive thermoelectric system with photovoltaic (PV), frictional nanogenerators (collecting energy from raindrops),²⁷ are potential strategies for achieving stable and continuous power generation. For instance, Chen et al. designed a biomimetic metafilm that achieved sustainable power supply in unfavorable weather (Figure 15f).⁴⁸⁰

The commercial viability of radiative cooling-driven thermoelectric systems (RC-TESSs) depends on transitioning from idealized laboratory setups to robust, scalable manufacturing. Current progress in large-area screen-printing of thermoelectric arrays and the use of biomass-based materials offers a clear pathway to reduce cost drivers while ensuring environmental sustainability. However, reliability and lifetime in real-world environments remain significant hurdles. Performance is often degraded by application-specific barriers, such as high thermal contact resistance at the device-skin interface in wearable textiles and restricted radiative view factors in dense urban building envelopes. To bridge this gap, representative solution pathways involve developing advanced, flexible interface materials with high thermal conductivity to minimize impedance, and optimizing device orientation to maximize sky exposure. Furthermore, the deployment maturity of RC-TES can be significantly enhanced by synergistic integration with other energy harvesters, such as PV for daytime boost or triboelectric nanogenerators for rainy conditions, evolving into all-weather power units. Such maintenance-free, self-powered systems are approaching readiness for critical low-power applications, including remote IoT sensors and implantable medical devices.

Overall, the autonomous energy-harvesting capability of RC-TESSs positions them as transformative power solutions for low-energy electronics, ranging from wireless IoT sensors to wearable health monitors.^{481,482} To bridge the gap between laboratory-scale demonstrations and practical deployment, future research must shift from maximizing theoretical efficiency to mitigating the dominant loss terms inherent in real-world

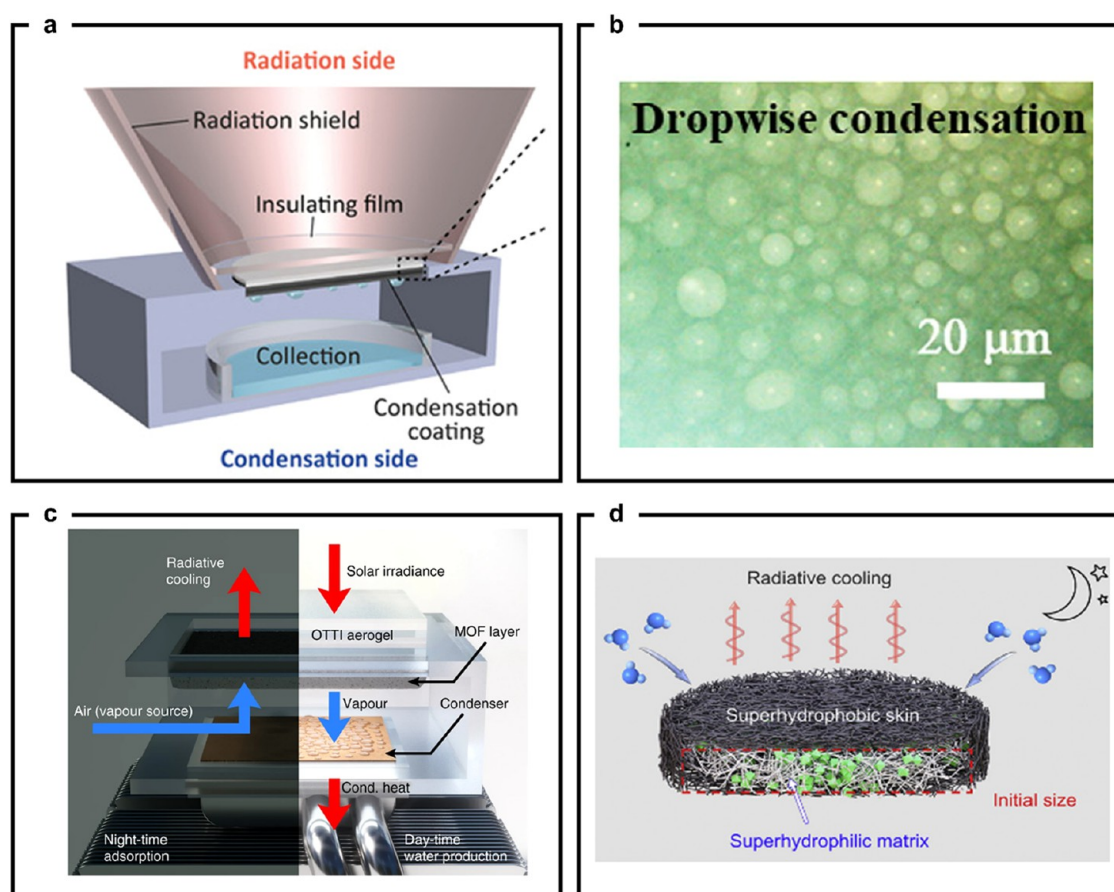


Figure 16. Radiative cooling applications for atmospheric water harvesting via direct condensation or adsorption assistance. (a) Working principle of the RCon with separated radiation and condensation side, where the radiation shield can substantially improve the dew harvesting potential. Reproduced with permission from ref 35. Available under a CC BY-NC 4.0 license. Copyright 2021 The Author(s). (b) An image of dropwise vapor condensation on a hydrophilic-superhydrophobic patterned surface (F-SiO₂/TiO₂, 1:3 w/w). Reproduced with permission from ref 491. Available under a CC BY-NC-ND 4.0 license. Copyright 2021 The Author(s). (c) Working principle of the RC-assisted SAWH system using MOF-801 with night-time adsorption (left half) and day-time solar-assisted water production (right half), where the OTTI aerogel suppresses convective heat loss from the solar absorber. Reproduced from ref 495. Available under a CC BY 4.0 license. Copyright 2018 The Author(s). (d) Schematic of the bioinspired heterogeneous wetting AWH device with fibrous skin for night-time RC-assisted sorption. Reproduced with permission from ref 496. Available under a CC BY-NC-ND 4.0 license. Copyright 2022 The Author(s).

environments. In particular, the thermal contact resistance at the device-source interface is a critical bottleneck for the conformal integration of wearable textiles, while the radiative view factor often limits performance due to complex installation geometries. Addressing these challenges requires a synergistic approach: developing advanced interface materials with high thermal conductivity and mechanical flexibility to minimize impedance, while simultaneously optimizing device orientation and spectral selectivity (8–13 μm) to maximize sky exposure. By integrating these adaptive configurations with complementary energy-harvesting modalities, such as photovoltaics or triboelectric nanogenerators, RC-TESs can evolve into robust, all-weather power units. Such advancements will facilitate the realization of truly maintenance-free, self-powered electronics, extending their applicability to critical systems like implantable medical sensors and remote environmental nodes.

5.6. Atmospheric Water Harvesting

Shengxi Bai, Kaixin Lin, and Chi Yan Tso

With freshwater resources dwindling with population growth, urbanization and climate change, RC has emerged as a promising approach for enabling AWH. This technology offers solutions for decentralized freshwater production, particularly in

water-scarce regions where freshwater transport and delivery are challenging. AWH holds great potential for alleviating water stress, given the vast amount of water vapor in the atmosphere (12,900 km³ fresh water).⁴⁸³ Among AWH methods, dew water collection stands out as more viable than cloud seeding or fogwater collection due to its cost-effectiveness and lower dependence on geographical conditions.⁴⁸⁴

RC can facilitate dew water collection either directly through dew-point condensation or indirectly by coupling with other AWH systems. First introduced in the late 20th century,⁴⁸⁵ radiative condensers (RCons), as a direct method, employ a subambient cooling surface to achieve direct water condensation at the dew point. Theoretically, RCons are engineered with high solar reflectivity and strong MIR emissivity to maximize radiative condensation power. Common designs include porous polymers, metamaterials, multilayer structures or randomly distributed structures.⁴⁸⁶ Unlike conventional RC designs that require selective infrared emission for subambient cooling, RCons leverage broadband infrared emission from 4 μm to over 13 μm . As the water vapor generated in most passive AWH systems is at or above ambient temperature, broadband infrared

emission maximizes radiative heat dissipation to the atmosphere and thus enhances radiative condensation.⁴⁸⁷

Several RCon designs and applications have been reported in recent years. Zhou et al.⁴⁸⁷ developed an RCon composed of a PDMS layer, a silver layer, and an aluminum plate to passively accelerate water vapor condensation. By pumping humidified air (RH = 90–95%) at ambient temperature into the condenser, the device achieved a daily water production of 0.8 mL with a surface area of 0.05 m² at UW–Madison in September 2017. Based on coalescence-induced water removal mechanism, Haechler et al.³⁵ demonstrated uninterrupted 24-h AWH by integrating thermal radiative shielding and cooling with a superhydrophobic RCon (Figure 16a). The radiative shield minimizes absorption of horizon-sourced atmospheric radiation while directing thermal emission toward low zenith angles, to optimize cooling efficiency. The system achieved a mean dew mass flux of 50 g m⁻² h⁻¹ under high humidity (RH > 90%) and moderate solar irradiation (>200 W m⁻²) conditions during the field tests at ETH Zurich in August 2019. Apart from standalone operation, RCons can be integrated with other AWH systems, such as sorption-based AWH (SAWH) systems. SAWH systems capture water vapor from ambient air using hygroscopic sorbents, release it via heating/regeneration (desorption), then condense the vapor into liquid water. Bai et al.^{488,489} demonstrated a dual single-bed SAWH system using MIL-101-Cr (HF) sorbent materials and poly(vinylidene fluoride-co-hexafluoropropylene) [P(VdF-HFP)] RCons for decentralized freshwater production. Such system could achieve a water condensation productivity of 678 mL m⁻² per day during clear days in Hong Kong based on field test results.

Apart from the investigation on radiative condensation power, more research is needed on the surface wettability modification to facilitate condensate collection. Dai et al.⁴⁹⁰ proposed that multifunctional coatings favorable for both droplet nucleation and removal can greatly improve AWH efficiency, and demonstrated a hydrophilic directional slippery rough surface for rapid nucleation and water droplets removal. Chen et al.⁴⁹¹ developed a wettability and spectral selectivity engineered coating using hydrophobic SiO₂ and hydrophilic TiO₂ nanospheres for efficient water collection. This surface wettability modification enhanced dropwise collection to a maximum droplet harvesting rate of 1047 mg cm⁻² h⁻¹ (Figure 16b). Bioinspired approaches show particular promise for advancing condensate collection. By mimicking biological structures, researchers aim to achieve mesoscale droplet nucleation and condensation and enable efficient water collection at macroscales. However, this remains a significant challenge. Wang et al.⁴⁹² suggested that multidimensional bionic structure design⁴⁹³ could be an effective approach, potentially promoting bionic AWH.

As an indirect method, RC can enhance dew water collection when integrated with other AWH systems. One typical example is utilizing RC to provide cooling effect during sorption process to maintain optimal RH, as the exothermic nature of moisture capture typically reduces sorption capability due to increased local temperature and decreased local RH.⁴⁹⁴ The potential of RC in improving the sorption efficiency has been demonstrated by several studies. Kim et al.⁴⁹⁵ developed a SAWH device using metal–organic framework (MOF)-801, employing night-time RC to lower the adsorber layer temperature and thereby increase the effective RH to facilitate water vapor uptake (Figure 16c). This approach reduced the temperature by ~3 °C during adsorption phase, increased the RH by 5–7% near the MOF

layer, and resulted in an equilibrium water uptake of 0.25 kg kg⁻¹. Similarly, Wang et al.⁴⁹⁶ utilized the RC properties of the carbon black-doped P(VdF-HFP)/polydimethylsiloxane fibrous skin to increase the effective RH during sorption. This modification accelerated the sorption rate and increased the water uptake capacity of their composite sorbent (i.e., active carbon felt-lithium chloride) (Figure 16d). Recently, Huang et al.⁴⁹⁷ demonstrated a passive SAWH system coupling composite hydrogel with RC and solar heating. Their field test showed that RC increased the night-time water uptake rate from 0.242 kg m⁻² h⁻¹ (using the sorbent only) to 0.310 kg m⁻² h⁻¹ (using both the sorbent and RC), representing a great performance improvement.

From an implementation perspective, industry analyses estimate the AWH market's base valuation at USD 2.8 billion in 2024, and it is expected to grow at a compound annual growth rate of 8% from 2025 to 2034.⁴⁹⁸ Cost-effective AWH powered by RC is still under investigation. Li et al. proposed an RC fabric for AWH with an estimated annual water production cost of \$5.2/L at 60% RH and \$0.01/L at 90% RH.⁴⁹⁹ Regarding reliability and lifetime in real environments, more attention should be paid on the optical degradation from UV thermal aging and surface soiling of RC materials. Compared with traditional AWH designs, RCon increases water collection in low RH environments and reduces system energy consumption, which offers an environmentally friendly and sustainable AWH solution.⁵⁰⁰ However, RC performance relies on weather and climatic conditions, which limits the applications of RCon and RC-assisted sorption process. The key application-specific barriers include low specific yield and sorption kinetics mismatch, parasitic heat gains and atmospheric transmittance. Certain progress has been made regarding these barriers, such as angular shielding and enhanced spectral selectivity, continuous 24-h transmissive RC architectures. Currently, AWH by RCon and RC-assisted sorption process remains heavily constrained by complex synthesis costs, operating primarily at the pilot scale.

Overall, RC contributes to AWH via two primary mechanisms: directly by condensing water using RCons and indirectly by enhancing sorption in SAWH systems. While RC-assisted SAWH systems generally demonstrate higher specific water productivity due to the utilization of hygroscopic sorbents and larger condensation capacity, RCons offer the distinct advantage of completely passive operation under suitable weather conditions. Current limitations of RCons, particularly their relatively low water productivity and efficiency caused by insufficient RC capacity and substantial heat loss,^{484,501} highlight the need for more research efforts. Future research could focus on developing advanced RCon materials with optimized radiative properties, improving condenser designs to enhance condensation efficiency and refining surface structures to maximize water collection performance. For RC-assisted SAWH systems, research priorities should include optimizing sorption efficiency through careful material selection of both RC coatings and sorbents, as well as adjusting system-level parameters tailored to specific climatic conditions. Addressing these challenges will be crucial for advancing both approaches toward practical implementation in water-scarce regions, offering sustainable solutions to global water stress.

5.7. Passive Isothermal Film

Seonggon Kim and Yong Tae Kang

Radiative coolers typically operate by reflecting solar energy in the ultraviolet, visible, and near-infrared regions during the

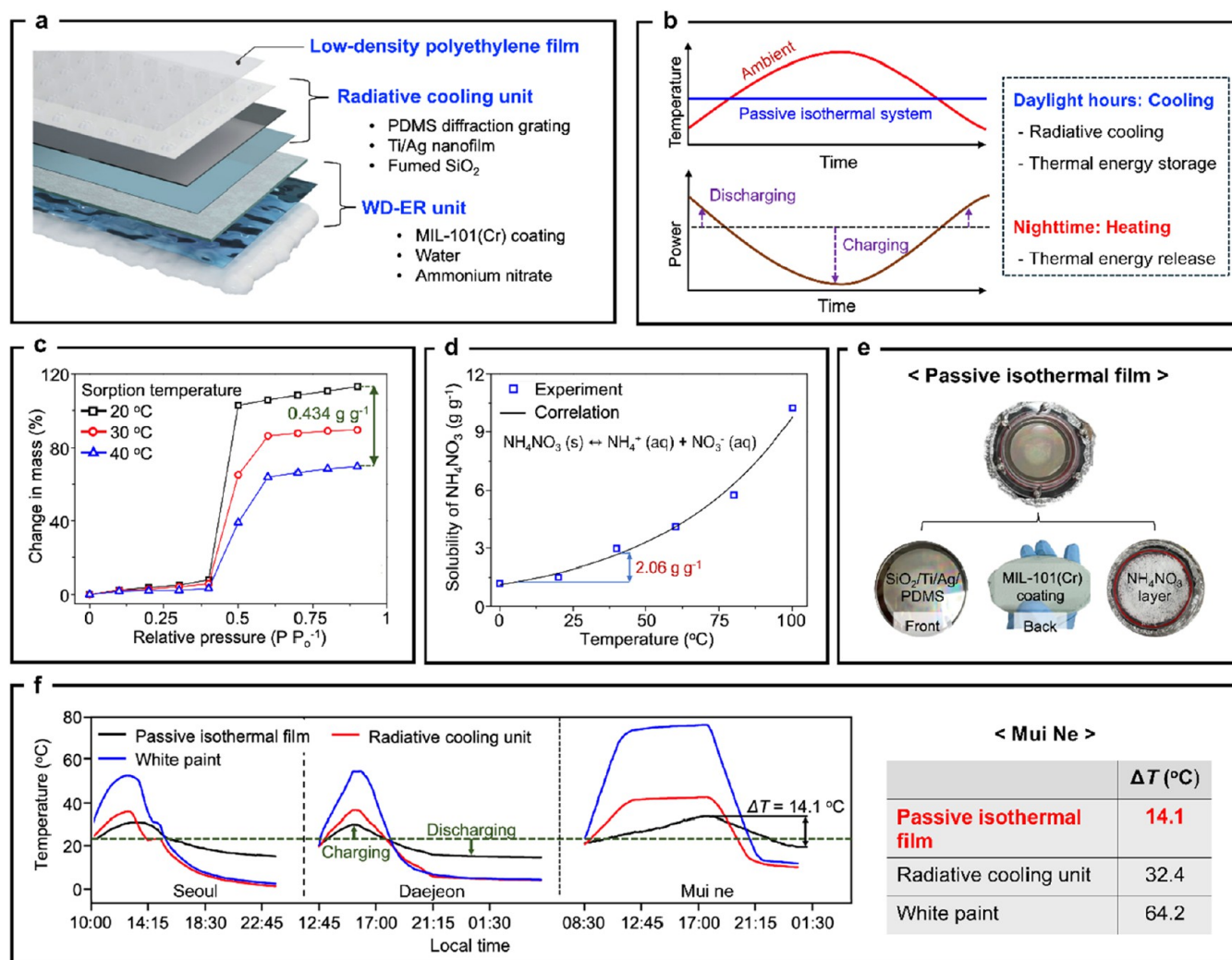


Figure 17. Radiative cooler-based passive isothermal film for arid climate applications. (a) Schematic of the system configuration, consisting of RC and water desorption-driven endothermic reaction (WD-ER) layers. (b) Idealized cooling and heating operations for maintaining an isothermal temperature of 25 °C over a full day. (c) Water adsorption isotherm of chromium(III) terephthalate metal-organic frameworks (MIL-101(Cr)). (d) Temperature-dependent solubility curve of ammonium nitrate. (e) Photographs of the passive isothermal film. (f) Temperature profile of the passive isothermal film throughout a full day. Adapted with permission from ref 502. Available under a Creative Common CC BY 4.0 License. Copyright 2024 The Author(s).

daytime while emitting thermal radiation in the mid-infrared to achieve subambient temperatures. Recent advances have enabled practical applications through cost-effective material designs such as hierarchically structured poly(methyl methacrylate),¹⁹⁷ polydimethylsiloxane-coated metal structures,²⁷⁶ delignified wood,¹⁵⁰ and three-dimensional porous cellulose acetate matrices with internally deposited SiO₂.¹⁷⁴ However, continuous thermal emission could increase heating loads rather than provide a benefit in cold climates or during nighttime in regions with large diurnal temperature variations, which limits the applicability of radiative coolers. In response to this challenge, temperature-responsive materials capable of self-switching thermal emission have been proposed as a means of selectively enabling cooling only when needed.^{307,309}

A radiative cooler-based passive isothermal film has been developed to reduce both cooling and heating energy consumption in arid climates with large diurnal temperature variations, maintaining 25 °C solely through natural processes without any external energy input,⁵⁰² as presented in Figure 17a. This film is composed of a low-density polyethylene cover, a RC

unit containing PDMS with a diffraction grating and fused SiO₂/Ti/Ag sublayers, and a water desorption-driven endothermic reaction (WD-ER) unit including chromium(III) terephthalate metal-organic frameworks (MIL-101(Cr)) and ammonium nitrate.

During daylight hours as illustrated in Figure 17b, the low-density polyethylene layer minimizes forced/natural convection heat transfer through intermittent air. The PDMS diffraction grating allows solar irradiation to pass through, while the SiO₂/Ti/Ag layers reflect it to prevent overheating. The PDMS diffraction grating is designed to achieve an emissivity close to 1.0 within the temperature range of 30–60 °C (typical of daytime temperatures in arid climates). The WD-ER unit absorbs the net thermal energy input through a chain reaction involving water desorption from the MIL-101(Cr) coating layer for latent cooling and an endothermic reaction by the dissolution of ammonium nitrate in water. This process sustains indoor temperatures by utilizing the principles that the water sorption capacity of porous materials decreases as temperature increases, and the solubility of solutes rises with temperature.

During nighttime, when the PDMS diffraction grating is exposed to lower outdoor temperatures than indoors, its emissivity decreases, minimizing thermal emission heat loss. Additionally, the reverse reaction in the WD-ER unit releases heat, which aids in temperature maintenance. While conventional passive RC systems focus on minimizing solar irradiation (reducing absorptivity in the ultraviolet–visible range) and enhancing thermal emission power (achieving emissivity close to 1 in the infrared spectrum), in this study, some energy input from nature is utilized to operate the WD-ER unit to store energy during daylight hours. This enables the passive isothermal system to discharge the stored energy during nighttime, which minimizes heating and cooling energy loads in arid climates by utilizing the diurnal energy balance.

Figure 17c presents the isothermal water sorption capacity of MIL-101(Cr). As the passive isothermal film operates in a moisture-containing environment, the capture capacity depending on the temperature variation is examined at a point where the relative pressure is close to 1. MIL-101(Cr) in the WD-ER unit exhibits a water sorption capacity of 1.12 g g^{-1} at 20°C , and as the temperature rises to 40°C , approximately 0.434 g g^{-1} of water is desorbed (This value is calculated from the chemical equilibrium state. However, the WD-ER unit operates in a quasi-steady state with a full-day cycle.). Linear regression of the isothermal water sorption capacity enables the prediction of working capacity with respect to temperature changes. The average water desorption enthalpy reaches 53 kJ mol^{-1} . Figure 17d displays the solubility of ammonium nitrate in water as a function of temperature. The dissolution enthalpy for ammonium nitrate is 28.1 kJ mol^{-1} , and its solubility can be fitted with an exponential function.

The configuration of the passive isothermal film is summarized in Figure 17e. Ammonium nitrate crystals were dispersed onto a waterproof surface, and a moisture environment was formed. A $\text{SiO}_2/\text{Ti}/\text{Ag}/\text{PDMS}$ film coated on the back with MIL-101(Cr) was attached to the $\text{H}_2\text{O}/\text{NH}_4\text{NO}_3$ layer. The temperature variation of the passive isothermal film was tested throughout a full day under various climatic conditions, as presented in Figure 17f. As a result of the experiment in Seoul, the temperature of white paint increases to 52.5°C during daylight hours and drops to 0.8°C at night. The maximum temperature of the RC unit is 35.8°C , which is 16.7°C lower than that of the white paint. However, a significant heating load is still required to achieve 25°C at night. The passive isothermal film demonstrates a reduction of 4.8°C in the maximum daytime temperature compared to the RC unit while presenting a significant increase in nighttime temperature by 13.6°C . The relatively large temperature difference of 17.5°C is attributed to the difficulty of preserving equilibrium between the charging and discharging of the WD-ER unit, especially due to the relatively short daytime duration in the test region compared to nighttime.

The results from tests conducted at the White Sand Dunes in Vietnam (Mui Ne) indicate that the temperature of white paint rises to 76.0°C during daylight hours and drops to 11.8°C at night, resulting in a temperature difference of 64.2°C . Although the RC unit reduces the maximum temperature to 42.5°C , the minimum temperature at night is lower than that of the white paint due to thermal emission. The passive isothermal film significantly reduces the maximum temperature difference to 14.1°C and generates a cooling power of -1.1 kW m^{-2} during the daytime and a heating power of 0.28 kW m^{-2} at nighttime (The cooling and heating power of the passive isothermal film

was obtained by calculating the power required to maintain the temperature difference between the indoor air in the system with a white paint surface and that with the passive isothermal film). By integrating the heating and cooling power generated throughout a full day and adding the solar energy absorbed by the white paint, the diurnal energy balance is established with an error margin of 9.7%.

RC-based isothermal film hold promise as a viable passive thermal management solution, particularly for buildings in arid or high-insolation regions. When integrated into building skins such as roofs or exterior panels, these systems could contribute to heating, ventilation, and air conditioning energy savings without the need for active control.⁵⁰³ Their passive operation aligns with net-zero energy building goals and off-grid applications. Future work should explore architectural integration strategies, durability under long-term environmental exposure, and compatibility with existing construction materials to assess scalability.

The passive isothermal film combines a radiative cooling unit ($\text{SiO}_2/\text{Ti}/\text{Ag}/\text{PDMS}$) with water desorption-driven endothermic reaction unit (MIL-101(Cr)/ $\text{H}_2\text{O}/\text{NH}_4\text{NO}_3$). The main cost drivers are the multilayer optical coating and the use of metal–organic frameworks. In practice, scalable radiative cooling films and sorbents such as zeolites could reduce fabrication cost, while their selection can be optimized depending on the operating conditions. Regarding reliability and lifetime in real environments, the passive isothermal film was tested for multiple cycles in different regions including South Korea and Vietnam, demonstrating stable performance. Since the system is composed of stable materials, it is suitable for scale-up in real environments. However, system performance depends on local climate conditions such as diurnal temperature variation and solar intensity, and the limited flexibility of the passive isothermal film makes its application to curved surfaces difficult. To overcome these barriers, optimization based on the thermophysical properties of the materials may enable operation in a wider range of environments, while integration of small units into building envelopes may improve practical applicability. Although current demonstrations remain at the prototype level, the individual components are based on well-established materials, suggesting that, with scalable fabrication and improved durability, applications in building envelopes are feasible.

It is also essential to consider alternative materials within the WD-ER unit to improve economic feasibility. Zeolites such as 13X, 5A, 3A, Y, SAPO-34, and SSZ-13 offer lower-cost, scalable options with reasonable water sorption performance.⁵⁰⁴ Similarly, alternative salts like NH_4Cl or KCl , could still provide useful thermal buffering effects when coupled with appropriate sorbents. Additionally, recent advances in low-cost RC designs, such as delignified wood structures or polymer-based multilayers, could be integrated to reduce fabrication complexity and material costs. These substitutions, if optimized for performance and reliability, would facilitate broader deployment in cost-sensitive or resource-limited settings.

5.8. Global- and Regional-Scale Artificial RC

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Global warming is caused by the decreased atmospheric transparent window caused by anthropogenic greenhouse gas emissions. Although it is urgent to decarbonize all energy sectors and eventually reverse the CO_2 level back to the preindustrial period, human civilization may not have enough time to prevent

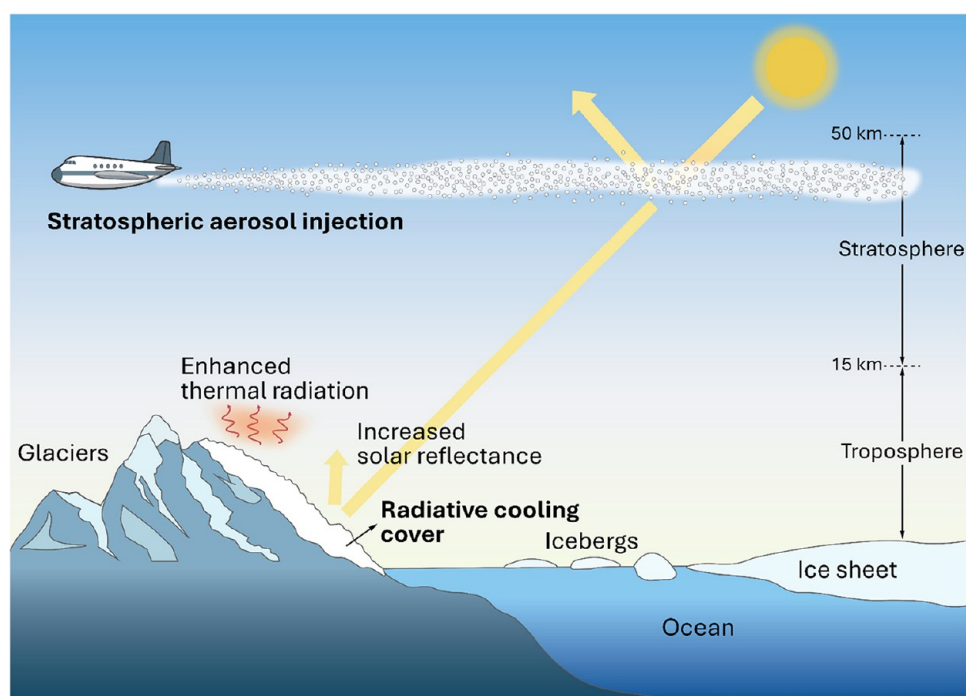


Figure 18. Schematic showing the artificial radiative cooling at the regional and global scales.

the catastrophic impact of global climate change if we only rely on decarbonization. Just like passive daytime radiative cooling is widely employed to enhance cooling without work input, there are emerging research efforts to conduct artificially enhanced radiative cooling at the regional or even global scale. Theoretically, mitigating the solar heat gain can have a more drastic effect than increasing the radiative heat loss (by restoring the atmospheric transparent window via decarbonization), making it a critical approach that warrants more scientific research and discussion. This Chapter will focus on two topics: glacier preservation and solar geoengineering (Figure 18).

5.8.1. Glacier Preservation. Glaciers, which cover approximately 10% of the Earth's land surface, hold profound geological, biological, and economic importance.⁵⁰⁵ However, the continuous increase in greenhouse gas emissions has led to an unprecedented rate of glacial melting since the beginning of the 21st century. This has resulted in an estimated annual mass loss of 260 gigatons between 2003 and 2009.⁵⁰⁶ Predictions indicate that by 2100, glaciers could lose approximately 26% of their 2015 mass, contributing to a mean sea-level rise of about 90 mm.⁵⁰⁷ This projection assumes an optimistic scenario where the global temperature increase is limited to 1.5 °C, a target that appears increasingly unlikely under current conditions.⁵⁰⁸ The accelerated retreat of glaciers not only raises sea levels but also threatens freshwater supplies, compromises the security of infrastructure due to events like ice avalanches and glacial lake outbursts, and negatively impacts the tourism industry.⁵⁰⁹ In recognition of the urgency, the United Nations has designated 2025 as the International Year of Glaciers' Protection.

Since the early 2000s, considerable theoretical and experimental efforts have been made to develop methods for artificially slowing the melting of snow and ice to preserve glacier mass.^{510–515} Understanding the mechanisms behind these methods requires an analysis of the energy balance at the glacier surface. According to the energy balance equation:⁵¹⁶

$$Q_{\text{melt}} = Q_{\text{sens}} + Q_{\text{lat}} + Q_{\text{rad}}$$

Here Q_{melt} is the net energy available for melting, Q_{sens} is the sensible heat flux from convection and conduction, which accounts for 15–20% of the net energy. Q_{lat} is the latent heat flux from phase change of water, which is often negligible as it contributes less than 10% to the energy budget. The dominant term, Q_{rad} , is the net radiation, which accounts for 75–80% of the energy driving the melting process. It is the sum of net shortwave (Q_{SW} , 0.3–2.5 μm) and longwave (Q_{LW} , 8–13 μm) radiation:⁵¹⁷

$$\begin{aligned} Q_{\text{rad}} &= Q_{\text{SW}} + Q_{\text{LW}} \\ &= (1 - R_{\text{solar}})Q_{\text{SW,in}} + (Q_{\text{LW,in}} - \epsilon_{\text{IR}}\sigma T^4) \end{aligned}$$

Here R_{solar} is the solar reflectance in the shortwave band (albedo), Q_{SW} and $Q_{\text{LW,in}}$ are the incoming radiation in the shortwave and longwave bands, respectively. ϵ_{IR} is the emissivity in the longwave band, σ is the Stefan–Boltzmann constant and T is the surface temperature in K.

Early glacier preservation efforts focused on increasing surface albedo. A glacier's albedo varies significantly: fresh snow exhibits a high albedo of 0.8–0.9, whereas the albedo of clean ice drops below 0.4. The accumulation of dust and debris further reduces albedo.^{516,517} Therefore, artificially creating a layer of fresh snow is a simple yet effective method to enhance reflectivity. For instance, a natural summer snowfall on the Morteratsch Glacier (Switzerland) in July 2000 resulted in a net preservation of 13 cm water equivalent by the end of the melt season.⁵⁰⁹ Similarly, an artificial snowfall experiment in the Altai region of China during summer 2018 demonstrated a 40% reduction in glacier mass loss,⁵¹⁸ further demonstrating the effectiveness of this method. However, this method is limited by its reliance on a substantial water source and a narrow window of favorable weather conditions for snow production.

To overcome these challenges, researchers have explored using high-albedo blankets, known as geotextiles, to cover glaciers. A 2012 experiment on the Presena Ovest Glacier (Italy)

demonstrated a 69% reduction in snow and ice melt in areas covered by a nonwoven polypropylene geotextile compared to uncovered areas.⁵¹⁹ This success was attributed to the geotextile's high mean albedo (0.64) versus the bare ice surface (0.43). The long-term effectiveness of the geotextile for glacier protection was confirmed by 15-year study in Switzerland.⁵²⁰ The result showed that coverage of glaciers using geotextiles can reduce the ice melt up to 350,000 m³ per year, corresponding to a 59% efficiency in ice melt reduction. With their effectiveness demonstrated in field tests, geotextiles have already been commercialized and widely used in glacier protection projects. However, most currently available geotextiles are made from petroleum-based polymers such as polypropylene and polyester, raising concerns about potential environmental impacts, particularly when deployed at large scale. In addition, the solar reflectance (albedo) of these materials is only moderate, suggesting that further improvements in reflectivity could enhance their overall cooling performance and melt-reduction efficiency.

A significant advance occurred in 2014 with the demonstration of passive radiative cooling, achieving temperatures ~5 °C below ambient even under direct sunlight.²⁴ This was accomplished using a multilayer photonic structure with a solar reflectance of 0.97 and strong thermal emissivity. However, the complex structure consisting of alternating nanometer-precision layers of HfO₂ and SiO₂ makes large-scale application impractical, as fabricating such a device in a cost-effective manner is highly challenging. Consequently, research has focused on developing more scalable materials with similar properties.

In 2022, Li et al. designed a hierarchical film based on cellulose acetate (CA), an abundant and eco-friendly material.⁵²¹ This film's porous structure yields a solar reflectivity of 0.974, while the vibrations of molecular bonds provide a mid-IR emissivity of 0.92. These properties result in an excellent cooling power of up to 110 W m⁻² and enable the material to maintain a surface temperature below 0 °C for extended periods. In addition, the CA film is more hydrophobic compared to the traditional polypropylene and polyester geotextiles, which helps keep its surface clean from dust that would otherwise reduce reflectance. With its cooling performance, antisoiling properties, mechanical strength, biodegradability, and potential for scalable production, this CA film is a promising candidate for glacier protection. However, the fabrication of the CA film via electrospinning remains relatively energy-intensive and time-consuming, posing challenges for large-scale manufacturing. As a result, the current production cost is expected to be higher than that of conventional geotextiles.⁵¹⁷ In addition, the long-term durability and large-scale effectiveness of this material for glacier protection still require validation through field experiments. Further efforts to develop scalable and cost-effective fabrication processes will therefore be essential for its practical deployment.

The accelerated melting of glaciers demands urgent and effective intervention. Mitigation strategies have evolved from applying artificial snow to employing durable high-albedo geotextiles. The future of glacier preservation likely resides in advanced materials engineered for passive radiative cooling, which offer superior performance and environmental compatibility. Future work must focus on validating the large-scale efficacy of these novel materials and developing cost-effective manufacturing processes to enable their widespread deployment. Overcoming these hurdles will be crucial in the ongoing effort to protect Earth's vital ice reserves.

5.8.2. Solar Geoengineering. In recent decades, scientists have been discussing global-scale approaches that could rapidly stop the Earth temperature increase through solar radiation management (SRM), also known as solar geoengineering. SRM aims at cooling the Earth by reflecting a portion of incoming solar radiation back into space. Among the proposed techniques, stratospheric aerosol injection (SAI) is the most widely studied, which seeks to enhance the solar reflectivity of the upper atmosphere by introducing fine aerosol particles into the stratosphere (about 15–20 km in altitude).⁵²² The efficacy of SAI has been showcased in the volcanic eruption of Mount Pinatubo in 1991, which released about 20 million tons of sulfur dioxide into the stratosphere, forming reflective sulfate aerosols that cooled the global climate by ~0.5 °C for about a year.⁵²³ Essentially, SAI is to artificially create such volcanic effects by deliberate and controlled injection of aerosols into the stratosphere.

In the exploration of SAI, developing suitable aerosol materials is one of the major research focuses. It involves a comprehensive set of metrics spanning optical, microphysical, chemical, and environmental properties. The optical performance is mainly characterized by the single-scattering albedo (SSA), which quantifies the fraction of total extinction due to scattering rather than absorption. Materials with near-unity SSA and strong backscattering are preferred for maximizing solar reflectivity. Particle microphysics, including size distribution, coagulation, and sedimentation, govern both radiative efficiency and atmospheric residence time. Optimal particle radii of approximately 0.1–0.5 μm are predicted to maximize scattering efficiency while maintaining sufficient atmospheric lifetime.^{524,525} Particles smaller than about 0.1 μm scatter solar radiation inefficiently and are prone to rapid coagulation, whereas larger ones settle faster and absorb more infrared radiation.^{526–528} In addition to single-component particles, composite or coated aerosols have also been proposed to improve overall performance.^{528,529} As an example, a recent study suggests that a thin high-index shell enclosing a low-density core can boost solar reflectivity, which also greatly lowers mass and settling rate, thus increasing their lifetime in stratosphere.⁵³⁰ As for chemical and environmental aspects, the selected materials should minimize heterogeneous reactions and ozone impacts while remaining stable under high UV exposure, as well as exhibiting negligible toxicity or ecological disturbance after their deposition in the environment.

The leading candidate material for SAI is sulfur dioxide (SO₂) gas, which oxidizes to form sulfate aerosol droplets (H₂SO₄) in the atmosphere. Sulfate has a high solar reflectivity and, when largely distributed in the stratosphere, can significantly increase global albedo. However, sulfate aerosols provide surfaces for heterogeneous reactions that generate chlorine and bromine radicals and accelerate ozone depletion, as observed after the 1991 Mount Pinatubo eruption.⁵³¹ In addition, the non-negligible infrared radiation of sulfates can warm the stratosphere and disrupt its circulation, thereby influencing ozone distribution and global climate patterns.⁵³² These substantial side effects have motivated research on alternative aerosol materials, such as alumina (Al₂O₃) or calcite (CaCO₃). Compared with sulfates, injection of solid particles can largely avoid stratospheric heating and even counter ozone loss by neutralizing acidic compounds and suppressing chlorine radical formation.^{533,534} For example, a modeling study suggests that using CaCO₃ particles with a radius of 275 nm can reduce stratospheric radiative heating by roughly an order of magnitude

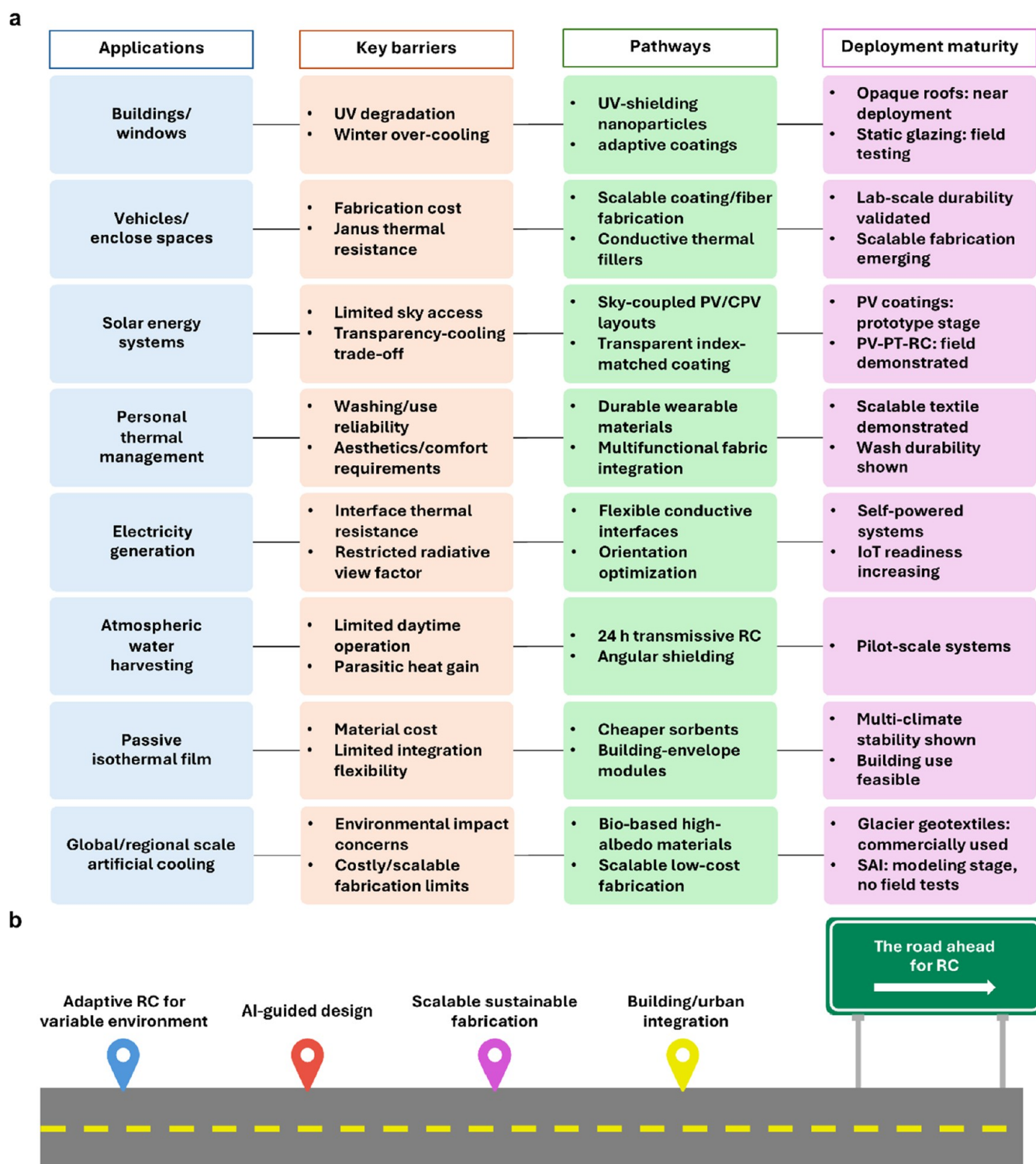


Figure 19. (a) Application-oriented roadmap of radiative cooling (RC) technologies, summarizing representative applications together with key barriers, corresponding pathways, and current deployment maturity. (b) Outlook roadmap highlighting future directions for RC.

compared with sulfate aerosols under the same radiative forcing (a benchmark for SRM performance).⁵³⁴ Among various SAI materials, diamond stands out for its high refractive index and low absorption coefficient, which ensures strong solar reflection and greatly limits stratospheric heating.⁵³² Although dispersing million tons of diamond would be economically infeasible, it serves as a benchmark for developing more advanced material candidates of SAI implementation.

In addition to technical challenges, such as determining what (e.g., aerosol materials),⁵³³ how (e.g., delivery methods),⁵³⁵ and where (e.g., injection locations)⁵³⁶ for SAI implementation, the major concern remains its potential global side effects.⁵³² The inevitable stratospheric heating can accelerate ozone depletion and change tropical atmospheric circulation. Moreover, SAI is expected to reduce the global mean precipitation. Historical observations after the Mt. Pinatubo eruption showed a

significant decrease in land precipitation and river discharge, suggesting a potential risk for widespread drought under SAI scenarios.^{537,538} Modeling studies show that many regions, especially monsoonal areas like Central India, could experience significant drying and reduced summer rainfall after SAI deployment.^{532,539} It is also noteworthy that SAI does not address the root causes of global warming — greenhouse gas emissions. Without effective and sustained CO₂ mitigation, a sudden termination of SAI would trigger an unprecedentedly rapid temperature rebound, posing severe risks to ecosystems and societies.⁵⁴⁰

Due to significant ethical and governance concerns, the real-world implementation of SAI has remained largely stalled. For instance, the Stratospheric Controlled Perturbation Experiment (SCoPEX) proposed by Harvard researchers planned a small-scale test in Kiruna, Sweden in 2021, but the experiment was finally canceled in 2024 after opposition from environmental groups and local stakeholders.⁵⁴¹ As a result, no stratospheric field experiment of SAI has been conducted to date, and most research remains confined to modeling and laboratory studies. The absence of field experiments means that many practical engineering challenges and potential environmental impacts remain unverified, which is considered one of the key factors limiting the further development and evaluation of SAI technologies.

Although being greatly debated due to its potential risks, SAI is regarded as perhaps the only feasible fast track for achieving the Paris Agreement's 1.5 °C temperature increase target.⁵⁴² Climate model experiments consistently show that SAI could induce rapid global cooling within just a few years of implementation, much faster than emission-mitigation methods.⁵³² Indeed, SAI is not intended to replace mitigation strategies, but rather to serve as a temporary emergency approach to quickly cool the planet and potentially buy time for effective emissions cuts to be fully implemented.

6. CHALLENGES AND FUTURE OUTLOOK

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While RC technologies have achieved remarkable progress in recent years, important challenges still remain to be overcome in order to fully realize their potential in research innovation and practical implementation. Figure 19a summarizes the application-oriented roadmap of RC by highlighting representative applications together with their key barriers, corresponding pathways, and current deployment maturity. Building on these practical considerations, this section discusses broader challenges and future directions for advancing RC toward real-world implementation and long-term impact.

- (1) The effectiveness of radiative cooling is strongly influenced by ambient factors such as humidity, cloud coverage, solar irradiance, and wind speed, which vary substantially across different regions and weather conditions. For example, high humidity can reduce cooling performance by absorbing mid-infrared radiation within the 8–13 μm transparency window.¹⁵ Cloudy skies also suppress radiative cooling. Although clouds reduce incoming solar radiation, they simultaneously enhance atmospheric re-emission in the infrared, which weakens the overall cooling effect.⁵⁴³ As a result, clear skies are generally required for radiative coolers to achieve their maximum performance. Such environmental variability highlights the need for radiative cooling strategies that

remain effective across different regions and weather conditions. One promising direction to address these challenges is the development of adaptable radiative cooling systems that can dynamically tune their optical and thermal properties in response to changing environments. Such adaptive systems can respond to diverse environmental stimuli, for example, temperature-adaptive RC^{222,307,317,544} and humidity-adaptive RC.^{267,310,373}

- (2) The use of artificial intelligence (AI) has become an increasingly powerful approach for accelerating and optimizing the design of photonic structures.^{545–547} AI techniques, including machine learning (ML) and optimization algorithms like genetic algorithms (GA) and particle swarm optimization (PSO), can efficiently explore large and complex design spaces by learning or evolving the relationships between structural parameters and optical responses.^{548,549} In the field of radiative cooling, these AI-driven approaches have started to play an important role in guiding design and performance optimization.⁵⁵⁰ For the optimization methods, PSO has been widely employed to optimize multilayer structures for achieving desired optical functionalities, such as in conventional RC²² and transparent RC.^{27,47,56} Similarly, GA is most often utilized for material selection and multilayer structure optimization in RC designs.^{21,102,551} ML has also emerged as an effective approach for the design and optimization of RC structures including multilayer,^{57,134,552,553} randomly distributed particle-based,^{554,555} and metasurface designs.^{119,152,153,556} For example, Zhang et al.¹¹⁹ adopt ML to inversely design hybrid metasurface-based thermal emitters with enhanced selectivity and wide-angle emissivity. Recently, several RC studies have combined optimization algorithms with ML to enhance design efficiency.^{553,555} For instance, Li et al.⁵⁵³ present a hybrid design framework that combines ML and GA to accelerate the discovery of high-performance multilayer RC structures, where GA explores the design space and ML guides the search toward the optimal configuration. This hybrid strategy is expected to play a key role in the future development of AI-assisted radiative cooling technologies.
- (3) Another key challenge for the broad deployment of radiative cooling technologies lies in the development of cost-effective, environmentally sustainable, and scalable fabrication methods. Despite significant progress in cooling performance, many state-of-the-art RC structures still rely on complex photonic structures, vacuum deposition, or lithographic techniques that are difficult to scale and costly to produce.^{47,56,476} Promising scalable pathways include films,^{52,557} paint-type coatings,^{33,78} and fabrics/textiles.^{176,236,457} However, their long-term durability under real-world conditions and mechanical robustness still need to be improved to ensure stable and reliable operation in practical applications. Furthermore, the use of biodegradable or naturally derived materials such as cellulose- or silk- based systems can help mitigate the environmental impact associated with polymer waste.
- (4) Lastly, a promising path for future development lies in integrating RC technologies into existing architectural and urban infrastructures. Embedding RC systems into building envelopes, windows, and roofs can provide passive thermal regulation and reduce energy consumption

tion without altering existing power systems. To achieve this, further efforts are needed to ensure mechanical durability, environmental stability, and aesthetic compatibility of RC materials under real outdoor conditions. The integration of scalable fabrication and adaptive control with infrastructure-oriented design will be key to realizing practical, building-integrated radiative cooling solutions.

The roadmap outlook of these perspectives is illustrated in Figure 19b.

7. CONCLUSION

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RC has rapidly evolved into a multidisciplinary field that bridges photonics, materials science, and thermal engineering. The research progress summarized in this mega-review highlights how RC has advanced from a fundamental concept to a versatile platform for sustainable thermal management and energy applications. In this article, we review the fundamental principles that govern RC, examine a wide range of structural designs and material systems, and discuss their diverse functionalities and emerging applications across various domains. Finally, we outline the key challenges and future perspectives that guide the continued development of RC toward practical, scalable, and environmentally sustainable technologies. We hope that this review serves as both a comprehensive reference and an inspiration for future research that will further expand the potential and impact of radiative cooling.

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Author Contributions

J.R. conceived the idea of a mega-review in radiative cooling. J.R. and H.K. outlined the mega-review structure. H.K. integrated parts for each section and conducted revision and editing. Sections ^{2.1} and ^{2.2}: J.P. and J.R. wrote the photonic concepts of RC and thermal balance of RC sections. Section ^{2.3}: H.L. wrote the representative fabrication strategies for the RC section. Section ^{3.1}: S.C. and S.S. wrote the multilayer thin-film structures section. Section ^{3.2}: C.L. and T.B. wrote the metasurfaces and nanophotonic architectures section. Section ^{3.3}: C.H., M.J., and D.L. wrote the porous structures section. Section ^{4.1.1}: Y.H., S.Z., and R.Z. wrote the monoselective RC emitter and dual-selective RC emitter sections. Section ^{4.1.2}: J.B. and M.K. wrote the transparent radiative cooler and colored radiative cooler sections. Section ^{4.2}: F.X., L.L., and W.L. wrote the directional and anisotropic RC section. Section ^{4.3}: X.Z., J.L., and K.D. wrote the adaptive and switchable RC section. Section ^{4.4}: S.D. and Q.G. wrote the hybrid and multifunctional RC section. Section ^{5.1}: S. Cao and Y.L. wrote the energy-efficient buildings and smart windows section. Section ^{5.2}: H. Kwak, D.H.K., and Y.M.S. wrote the vehicles and enclosed spaces section. Section ^{5.3}: J.B.Y. and D.R.K. wrote the high-performance solar energy systems section. Section ^{5.4}: Y. Hou and J.Z. wrote the personal thermal management section. Section ^{5.5}: Y. Hou and B.Z. wrote the electricity generation section. Section ^{5.6}: S.B., K.L., and C.Y.T. wrote the atmospheric water harvesting section. Section ^{5.7}: S.K. and Y.T.K. wrote the passive isothermal film section. Section ^{5.8}: Q.F., Q.L., and P.-C.H. wrote the global- and regional-scale artificial RC section. H.K. and J.R. wrote the abstract, introduction, challenges and future outlook, and conclusion sections.

Notes

The authors declare no competing financial interest.

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